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Non-LTE Radiation From an Argon Seeded Microballoon Implosion

I. INTRODUCTION

In this report, we will describe some results of calculations of Kshell emission from argon, seeded in the DT fuel of a microballoon that is imploded by high intensity irradiation from a CO2 laser. The argon is added to the DT in order to diagnose the extent of DT compression that is obtained by ablation of the outside microballoon materials (in the case described here, plastic-coated glass). One can then determine the compressed density by analyzing the emission profiles of the argon K-series lines for Stark effects caused by the mixing of states within the principal quantum number multiplets at high densities by electron collisions and ion electric microfields. The success of this analysis depends on a number of theoretical considerations: how well (1) the microfield distributions and the Stark profiles (2) the combined effects of electron impact excitation and ionization and of optical pumping on the ionization state of the argon, and (3) opacity corrections to the line emission profiles can be calculated. Moreover, one is also interested in how well the hydrodynamic implosion of the microballoon can be described and whether or not a post-processing of the predicted hydrodynamic behavior of the microballoon for the time integrated argon emission spectrum will agree with experimental observations. All of these issues are under investigation in this joint NRL/LANL program, and this final report will provide a status of achievements to date.

Efforts during the last year concentrated on several important tasks: (1) the calculation of Stark profiles for $L_{\alpha},\ L_{\beta},\ L_{\gamma},\ and\ L_{\delta}$ lines in hydrogen-like and helium-like argon (Ar XVIII and Ar XVIII respectively), (2) the coupling of these profiles to a calculation of the collisional-radiative ionization equilibrium state of argon, and (3) the use of diagnostic procedures that allowed comparison of the results of these calculations both to experimentally obtained argon K-series spectra and to the ionization state of argon as theoretically predicted by average ion models. The Stark profiles used in the emission spectrum calculations included both the effects of electron collisions and ion microfields as well as Doppler convolutions. The ionization calculations contained an extensive level structure and an

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extensive set of collisional and radiative couplings. Finally, the diagnostic procedures consisted of cell-by-cell monitoring of all ground and excited state populations densities and the calculation of time integrated emission spectra that included the additional effects of instrumental broadening.

A hydrodynamics LASNEX calculation carried out at LANL provided the description of the argon/DT implosion. Time histories of the central radii of the spherical shells, r(i,t), the total electron densities, $N_e(i,t)$, the electron and ion temperatures, $T_e(i,t)$, $T_i(i,t)$, and the total average charge states $\overline{Z}(i,t)$ (for each of the 11 cells describing the argon/DT core region of the microballoon, $i=1,\ldots,11$) were obtained from this calculation and used as input to the radiation-ionization calculations described in this report. Let α denote the (molecular) ratio of DT to Ar, which was 50 in these calculations. Since \overline{Z} is related to the total ion density, N_i , of D, T, and Ar ions by $N_e = \overline{Z} N_i$ and since N_i is related to the density of argon ions N_{Ar} by $N_i = (2 \alpha + 1) N_{Ar}$, the argon density was calculated from N_e and \overline{Z} by

$$N_{Ar}(i,t) = N_{e}(i,t) / \left[(2 \alpha + 1) \overline{Z} (i,t) \right]$$
 (1)

Argon emission spectra were computed for each time by approximately calculating the collisional-radiative equilibrium by solving the coupled, nonlinear set of equations ^{1,2}:

$$\sum_{i} V_{m\ell} (N_{\ell}, U_{\nu}) N_{\ell} (i,t) = 0 \quad m = 1, \dots, M$$
 (2)

$$\sum_{i} N_{i}(i,t) = N_{Ar}(i,t)$$
 (3)

$$N_{e}^{CRE} = \sum_{1}^{N_{\ell}(i,t)} (Z_{\ell} + 2\alpha)^{*}$$
(4)

[#] The LASNEX calculations invoked the XSNQ Non-LTE subroutine. See Ref. 25 for a description of XSNQ.

^{*} The electron density, $N_{\rm e}^{\rm CRE}$, is not necessarily equal to the quantity calculated by LASNEX, the latter is used <u>only</u> to obtain the argon number density (Eq. 1).

$$\left\{ \mu \frac{\partial}{\partial \mathbf{r}} + \frac{1-\mu^2}{\mathbf{r}^2} \frac{\partial}{\partial \mu} \right\} \mathbf{I}_{\nu}(\mathbf{i},\mu,t) =$$

$$\mathbf{k}(\nu,\mathbf{i},t) \left\{ \mathbf{S}(\nu,\mathbf{i},t) - \mathbf{I}_{\nu}(\mathbf{i},\mu,t) \right\}$$
(5)

$$U_{v}(i,t) = \frac{2\pi}{c} \int_{-1}^{1} d\mu I_{v}(i,\mu,t)$$
 (6)

for the argon population densities $\left\{N_{\hat{k}}\right\}$ and for the radiation energy densities $U_{\nu}(i,t)$ that couple to these populations. The emission spectrum $P_{\nu}(t)$ was also obtained from I_{ν} evaluated at the surface of the core region (i.e. no attenuation of this emission on passage through the glass or plastic was computed):

$$p_{V}(t) = 2\pi \int_{-1}^{1} d\mu \, \mu \, I_{V} (i = 12, \mu, t)$$
 (7)

In these equations, μ is the cosine of the angle between the radius vector and the ray of specific intensity \mathbf{I}_{ν} , \mathbf{Z}_{ℓ} is the charge of the ionization state ℓ , k and S are the absorption coefficient and source function respectively, and $\left\{\mathbf{W}_{m\,\ell}\right\}$ is the collection of rate coefficients describing the collisional and radiative couplings between the various states of the ionized argon.

An important part of the physics of Equations (2) – (6) is contained in the frequency dependence of the absorption coefficient and source function for the Lyman-series lines. For the H-L $_{\alpha}$, H-L $_{\beta}$, H-L $_{\gamma}$, H-L $_{\delta}$, He-L $_{\alpha}$, He-L $_{\beta}$, He-L $_{\gamma}$, and He-L $_{\delta}$ lines, these frequency dependences were calculated as the convolution of Doppler and Stark line profile functions. All higher members of the Lyman-series were assigned Voigt line profiles, with Stark width estimates. The Stark profiles that were used in these calculations are described extensively in the Appendix.

There are several ways to evaluate the self-consistency of these calculations. One is to note how closely the given electron density N_{μ} agrees

with the inferred electron density $N_e^{\ CRE}$. Another more detailed approach, which is presented in this report, is to compare the argon population densities that are obtained from the hydrodynamics calculations, which used average atom theory, to these densities as obtained from the CRE calculation. Finally, of course, one can compare calculated emission spectra to time integrated (or resolved) argon Lyman-series spectra that are measured in ${\rm CO}_2$ -microballoon compression experiments. Several examples of calculated time integrated emission spectra, showing the spectral detail that is possible, will be shown later in this report.

II. ATOMIC DATA

The spectra produced by the model is sensitive to the atomic data used, and the level structure and rates can be extended and improved as the need arises. Those used for the present calculations are as follows.

The atomic model contains all 19 ground states plus those excited states shown in Fig. 1 minus the five doubly-excited states which lie above the first ionization limit. Transitions from these doubly-excited states to their respective ground state produce the satellite lines to the resonance line of the next higher series. Since we were not focusing on these satellite lines in this calculation, the doubly excited states were, in fact, not used in the present calculation. These satellite structures can be incorporated into these calculations, as mentioned above as the need arises. Note also that many of the higher states are actually multiplets (or supermultiplets), the assumption being that collisions are fast enough to equilibrate the individual levels that have been included in the multiplet. The energy levels were obtained from the tables of Bashkin and Stoner³, Kelly and Palumbo⁴ and from scaling laws, for those high-lying states that are not tabulated. The ground and excited states of the ion of charge Z are coupled to the ground state of the Z + 1 ion by collisional ionization (calculated by the exchangeclassical impact parameter method), photo-ionization (hydrogenic crosssection with Karzas-Latter free-bound Gaunt factors'), and the collisional and radiative recombination rates obtained by detail-balancing the above. Adjacent ground states can be coupled by dielectronic recombination (although they were not, due to the omission of satellite lines from the present model). Each excited state of the ion Z is coupled by electron impact to the ground

state and other excited states of the ion Z. The excitation rates for transitions with principal quantum number n < 6 were calculated by the method of distorted waves 9,10 . The levels with n \geq 6 the rates were calculated by the semi-classical impact method. ¹¹ The collisional de-excitation rates were calculated by detail-balancing the corresponding excitation rates. Spontaneous decay rates were collected from a number of sources $^{12-16}$.

The broadband radiative coupling theory that is employed in this model has been described in detail elsewhere 1,17 . It includes a self-consistent treatment of the overlap of line and continuum absorption and emission processes, under the assumption that these processes detail balance in the sense that line emission and absorption profiles are identical. The number of radiative couplings used in the present argon model is more extensive than those employed earlier for aluminum 1 . They include principal Lyman series couplings in Ar XVII and XVIII from n=2 to n=10. With the inclusion of the intercombination line, $1s^2$ 1 S $-1s2p^3$ P, there are 19 line couplings in all in this model and no more. In addition, there are 8 continuum couplings: Z+H(n=1), Z+H(n=2), $H+He(1s^2$ 1 S), $H+He(1s2s^3$ S), $H+He(1s2p^3$ P), $H+He(1s2s^1$ S), $H+He(1s2p^3$ P), and $H+Le(1s^2$ 1 S) and 1 B 1

The initial conditions of the hydrodynamics calculation are shown in Figure 2. Six kilojoules of CO $_2$ laser energy with a pulse risetime of 392 psec. are used to drive the 350 μm diameter microballoon. The plastic coating is intended to shield the fuel region from electron preheat. This region, containing DT and argon, is initially 247 μm in diameter. It implodes to a minimum diameter of 32 μm at \sim 1160 psec. (roughly an eight-fold decrease in size). During this compression, peak temperatures are reached at approximately 1070 psec, and Argon K-shell emission substantially ends at around 1300 psec.

III. RESULTS: ATOMIC STATE NUMBER DENSITIES AND ORBITAL OCCUPATION NUMBERS

In Figs. 3-25 more of the details of the hydrodynamics calculations are shown; the solid line refers to quantities in cell No. 1 (the inner center cell), the dash-dot line, to quantities in cell No. 6 (the middle cell) and the dashed line to quantities in cell No. 11, (the outer cell). In Fig. 3 we show the radial distances to the center of each of these three cells as functions of time. Figure 4 shows the corresponding electron temperatures

while Fig. 5 contains the corresponding <u>argon</u> number densities (see equation 1). Notice as noted above that peak temperature precedes peak density by 0.1 ns. It is also worth noting that while the peak temperature occurs at the center (cell No. 1) the peak in density occurs at the outside (cell No. 11).

From these plasma conditions, we have computed the following ionization behavior for argon. The fractions of ions that are fully stripped is plotted in Fig. 6. Not surprisingly, these plots peak at the same time as the electron temperature. Next, Figures 7-10 are plots of the fraction of the argon atoms that are stripped down to one electron. In Fig. 7 the remaining electron is in the ground state, while it is in the state with n = 2,3 and 4 in Figs. 8-10. These plots again peak at the time of peak electron temperature. Finally, the fractions of the argon atoms with two bound electrons are plotted in Figs. 11-17. Since the temperature to remove the last L-shell electron (ionize Ar XVI) is much lower than the peak temperature achieved (1 keV), ground state Ar XVII is abundant during the early part of the calculation and is drastically reduced near peak temperatures, (See Fig. 11). On the other hand the temperature necessary to excite an n = 1 electron is of the order of a keV so the excited states of Ar XVII do not become prevalent until the time of peak temperature, at this point the density is increasing and the excited states thus track the density profiles rather than the temperature (see Figs. 12-17). As stated above the energy to ionize Ar XVI is quite low, thus its abundance is low throughout much of the calculation but does build up a bit during the reexpansion of the plasma, (See Figs. 18-21).

A simpler "Average Atom" model of the atomic structure was used in the hydrodynamics calculation. In such models one does not distinguish to which nucleus a given electron is bound, or, more precisely, whether other electrons are or are not bound to the same nucleus. One only determines a distribution of quantum numbers of the bound electrons. Thus one calculates the number of "2p orbitals" (per nucleus) that are occupied. Or if one is satisfied with even less detail, one calculates the number of "n = 2 orbitals" (per nucleus) that are occupied.

The orbital occupation numbers, \emptyset_k can be calculated from our fractional population numbers as follows: Denote by f_{ij} , the fractional population of the ion with i bound electrons in the j-th excited state. The excited states are ordered by excitation energy and j = 0 is the ground state.

$$\phi_{1s} = f_{1,0} + 2 \sum_{i=2}^{18} f_{i,0} + \sum_{j=1}^{13} f_{2,j} + 2 \sum_{j=1}^{7} f_{3,j} + f_{3,8}$$

$$\phi_{2s} = f_{3,0} + 2 \sum_{i=4}^{18} f_{i,0} + 1/4 f_{1,1} + f_{2,1} + f_{2,3} + f_{2,14} + f_{2,16}$$

$$\emptyset_{2p} = \sum_{i=5}^{18} \min (6,i-4) f_{i,o} + 3/4 f_{1,1} + f_{2,2} + f_{2,4} + f_{2,14} + f_{2,15}$$

$$+ f_{2,16} + 2 f_{2,17} + f_{3,1} + 2 f_{3,8}$$

$$\emptyset_{3s} = f_{11,0} + 2 \sum_{i=12}^{18} f_{i,0} + 1/9 \left[f_{1,2} + f_{2,5} + f_{2,6} \right] + f_{3,2}$$

$$\emptyset_{3p} = \sum_{i=13}^{18} \min (6,i-12) f_{i,0} + 3/9 \left[f_{1,2} + f_{2,5} + f_{2,6} \right] + f_{3,3}$$

$$\phi_{3d} = 5/9 \left[f_{1,2} + f_{2,5} + f_{2,6} \right] + f_{3,4}$$

$$\emptyset_{n=1} = \emptyset_{1s}$$

$$\emptyset_{n=2} = \emptyset_{2s} + \emptyset_{2p}$$

$$\emptyset_{n=3} = \emptyset_{3s} + \emptyset_{3p} + \emptyset_{3d}$$

$$\emptyset_{n=4} = f_{1,3} + f_{2,7} + f_{3,5}$$

where
$$\sum_{i,j} f_{ij} = 1$$
, $\emptyset_{n=1} \le 2$, $\emptyset_{n-2} \le 8$, $\emptyset_{n=3} \le 18$, etc.

The orbital occupation numbers are plotted in Figs. 22-25. Again, the solid line corresponds to the inner cell (#1), the dot dashed line to cell #6 and the dashed line to the outer cell (#11). On Fig. 22 we show the n = 1 orbital occupation; we have also plotted a few points calculated for cell #1 by LASNEX in the Average Atom approximation. The difference is of the order of 30%. This indicates discrepancies in these two ionization equilibrium calculations of the order of 30%!

In Fig. 23 the n = 2 orbital occupation data is plotted along with some LASNEX results for cell #1. The LASNEX and CRE differences in n = 2 orbitals are even larger! Since the x-ray emission calculations depend critically on the strength of emission and self-absorption as determined by the state occupation numbers, these discrepancies will have a marked influence on the use of the CRE or average atom calculations to carry out diagnostics. An interesting question as to the effect of these occupation number differences on x-ray energetics during compression remains to be investigated.

IV. RESULTS: SPECTRA

Time integrated spectra are presented for several times. In Fig. 26 we show the spectra integrated for t = .8 ns to 1.06 ns. The spectral region shown, 3.0 to 4.1 keV, contains all the strong K-shell lines that are measured and distinct at these densities. As stated in the introduction we do not as yet include the doubly excited states that would produce the satellites to the Ar XVIII L α and the Ar XVII L α -like resonance line. All the lines in Fig. 26 except the Ar XVII intercombination line and $1s6p \rightarrow 1s^2$ were calculated using the convolution of Doppler and Stark profiles. In addition approximate corrections have been included for the effects of ion-dynamics and microfields due to the fluctuations of the electrons in the screening cloud (see the Appendix for more details). The fine structure splitting of $L\alpha$ is larger than the Stark width at the electron density of these calculations. Since the fine structure splitting is of the order of the instrumental plus source broadening, so that the splitting cannot be resolved by this type of experiment, we convolved $L\alpha$ with an additional Gaussian whose width is the fine structure splitting. For this reason La appears relatively too wide on Fig. 26. In Fig. 27 the whole of the spectra has been convolved with a Gaussian profile whose width is equal to 7 m $\stackrel{ extstyle A}{ extstyle A}$, the combined instrumental plus source broadening. In Fig. 27 L α appears with a relative width much closer to those observed. In addition the apparent intensity of the intercombination line is reduced to normally seen levels, and some of the detailed features of the Stark profiles (central dips) are washed out.

In Figs. 28 and 29 these same spectra as obtained from time integrations from .8 to 1.18 ns are plotted. By comparing the intensities on Fig. 26(27) to those on Fig. 28(29) we note that L α and L $_{\beta}$ have increased more than the other lines, from which we conclude that the Ar ions have spent a (relatively) larger part of the time as Ar XVIII during the time between 1.06 to 1.18 ns (a fact that is confirmed by Fig. 7 and 11). Finally, in Fig. 30, we show the emission spectrum, fully formed, integrated out to 1.3 ns. Unfortunately an experimental spectrum for this 18 atm. fill case is not available for comparison at this time. A calculation for 30 atm. fill for which there are experimental spectra will be made in the near future, as soon as the LASNEX calculation is made available to us.

V. SUMMARY

We have described two sets of efforts that were successfully carried out this last year. One, which was brought to a fairly mature state, involves the calculation of emission profiles that are convolutions of Doppler and Stark profile functions for both one and two electron systems (Ar XVII and XVIII) from Lyman-lpha all the way to the Lyman- δ lines including both electron and ion contributions. The other effort to merge these Stark profile calculations with calculations of the implosion dynamics and argon x-ray emission behavior, on the other hand, has only recently been inaugurated. Hence, they are much less mature, yet they contain considerable potential. Nevertheless, in this latter effort, we have successfully demonstrated (1) that the fully developed theories and calculations of Stark broadening can be merged self-consistently with equally developed and detailed calculations of the collisional-radiative equilibrium state of the argon K-shell, (2) that in turn this full set of calculations can be utilized to post-process and analyze a partial set of LASNEX hydrodynamics data containing spatial gradients, and finally (3) that the result of these analyses can comprise a fairly complete set of predictions of both the emission spectrum and ionization state to compare against experimental observations and average atom theories.

Although the analysis described in this report dealt with a case for which no experimental data is presently available, it did provide some initial comparisons with the average atom predictions of LASNEX. CRE number densities were selfconsistently (to reasonable approximation) calculated along with the radiative emission. By forming the appropriate combinations of the fractional populations of the atomic states, we were able to calculate what would appear to be equivalent orbital occupation numbers. When these numbers were compared to the average atom quantities calculated directly by LASNEX it was found in this one case that a discrepancy exists. For the n = 1 orbital LASNEX and the CRE calculation differed by $\frac{2}{3}$ 30% while for the n = 2 orbital, the difference was a factor of $\frac{2}{3}$. Because the orbital occupation numbers are different it follows that the ionization/excitation level is also different, (i.e. the apparent differences in the conception of the two models lead to differences in consequences in this case).

The success of our efforts to date raises important questions that need to be addressed in the future. For example, the calculations described in this report were carried out with a minimum of time steps, using substantially the time steps required in the hydrodynamics calculations, which do not necessarily guarantee good CRE solutions nor accurate time integrations of the emission spectrum. A similar problem may exist because of the spatial gradients in temperature and density. More or better placed cells may be required in order to obtain an adequate resolution to these gradients for integration of the radiative transport equations. The atomic structure of our model is no doubt adequate, however, some of the important radiative couplings (eg. Balmer line couplings) may have been excluded from the model, as well as some of the important doubly excited state couplings. The present calculations also neglect the effects of the glass either to radiate and photoexcite the argon or to absorb and modify its K-shell emissions.

In future work the atomic model will be further enriched, in particular we will begin to work in the L-shell to investigate L-shell energetics. The K-shell Stark profiles will be improved with the addition of quantum mechanical strong collision terms, and the correction for the finite duration of collisions will be incorporated into the two electron code. Finally, we look forward to direct comparisons of the time intergrated K-shell spectrum to experimental spectra (as soon as the appropriate LASNEX simulation data is made available to us), and to much more detailed analyses of the differences in energetics and diagnostics between CRE and average atom theories than was given in the one comparison made in this report.

APPENDIX

VI. STARK PROFILES

The stark profiles used in the radiation transfer calculations were computed based on a theory which treats the electron collisions by an impact approximation that allows for the level splittings caused by the ion fields, the finite duration of the collisions, and the screening of the electric fields. The ion effects are calculated in a quasi-static, linear Stark effect approximation, using the electric microfield distribution functions of Hooper and Tighe which accounts for both correlation and shielding effects.

The profiles for Ar XVII and XVIII have already been discussed 19 . The modifications of the one electron calculation that were necessary to treat the He-Like profiles were also discussed 19 . The Ar XVIII profiles we use are the same as those in Ref. 19; however, it has subsequently been found, at least for argon, that L-S coupling is not an adequate approximation to determine level splittings. Instead, it was necessary to express the D, F, G, etc states as combinations of singlets and triplets. These energy levels and their mixing coefficients were obtained from the work of R. Cowan 20 and are summarized in tables 1-3. The effect of these mixed states on the profiles is shown in Figs. 31-34 (the solid line is the "mixed state" result, the dashed line is from the "singlet only" approximation).

The electron collision operator for a system of more than one bound electron is complex and one would like to look for ways of simplifying it. In Figs. 31-34 we show the effect of neglecting the imaginary (shift) part of the operator (points marked by circles). If in addition to this approximation a simplification that is often used in the evaluation of the real

^{*} The correction for the finite duration of collisions has not yet been implemented into the two electron code. (It will increase the expense of the calculations and the implementation has been delayed pending the inclusion of the correct quantum mechanical strong collision term.) The effect of the neglect of the finite collision time is only important for frequency deviations from line center larger than the plasma frequency. (For 1s5p-1s(2) the plasma frequency is near the half intensity point, so the wings of this line suffer larger errors than the rest of the profiles).

part of the operator ²¹ is used, one obtains the points marked by crosses. As can be seen, the imaginary part has a negligible effect and we subsequently ignore it. The simplification of the real part does not lead to a large error, but we retain the more correct form in anticipation of a larger correction once the quantum mechanical correction for the strong collisions has been extended to the two electron system.

A theory has been developed by Griem for the correction to line profiles due to the motion of the ions and to the fluctuations in the electric microfield caused by electrons in the Debye screening cloud. These effects have been evaluated for Lyman alpha ²² and Lyman beta ²³ lines, an approximate correction for these effects is to convolve the Stark profiles with a Gaussian whose width was discussed by Griem et al. ²⁴ Table 4 contains the appropriate Gaussian widths for the argon XVII and XVIII profiles.

In summary, the Stark profiles that were used in the calculations and described in the text are shown in Figs. 35-50 and Table 5-20.

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- 24. H.R. Griem, M. Blaha and P.C. Kepple, Phys. Rev. A 19, 2421 (1979).
- 25. W.A. Lokke and W.H. Grasberger, "XSNQ-U a Non-LTE Emission and Absorption Coefficient Subroutine," UCRL-52276, June 1977.

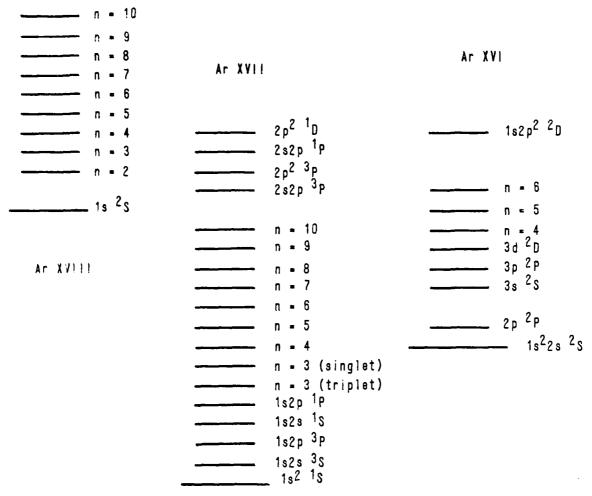


Fig. 1 - Energy level diagram for those levels included in the model

PELLET CONDITIONS

DT/ARGON PELLET: PARTICLE RATIO OF

DT-TO-ARGON: 50 to 1

FUEL RADIUS: 123.5 MICRONS

LASER: ENERGY = 6 KJ

RISETIME = 392 PS

ELECTRON TEMPERATURL: LASNEX

ELECTRON DENSITIES: LASNEX

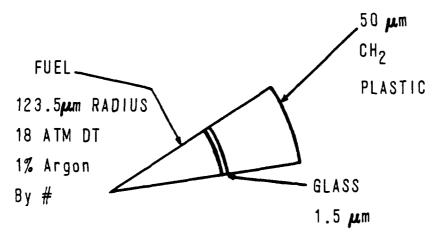


Fig. 2 — Pellet and laser conditions for the microballoon implosion modeled

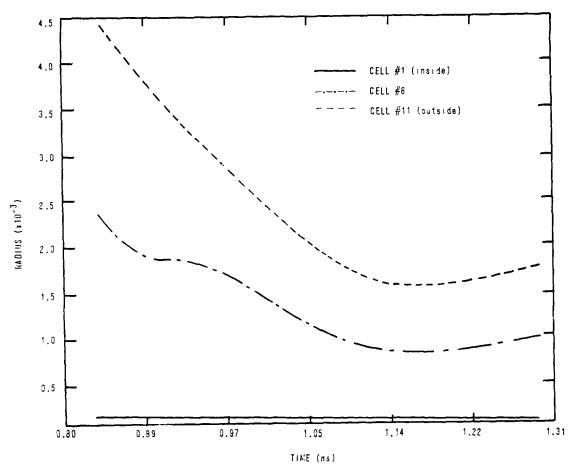


Fig. 3 - Radius of cell center vs time

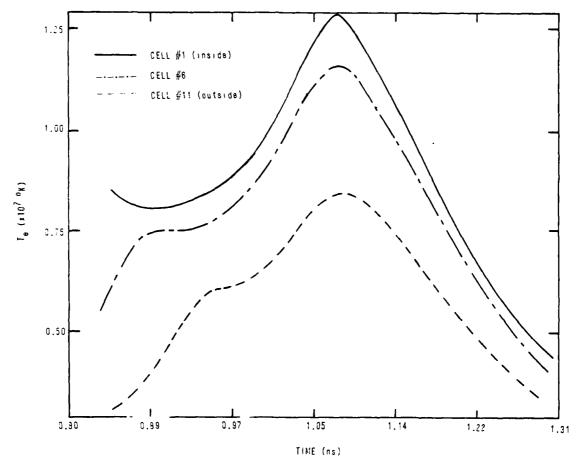


Fig. 4 — Electron temperature vs time

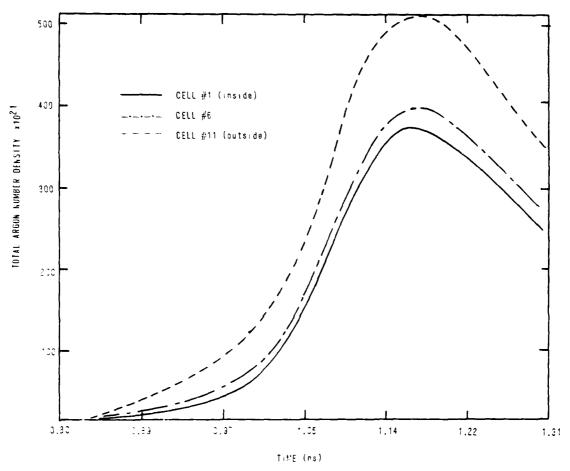


Fig. 5 — Total argon number density vs time

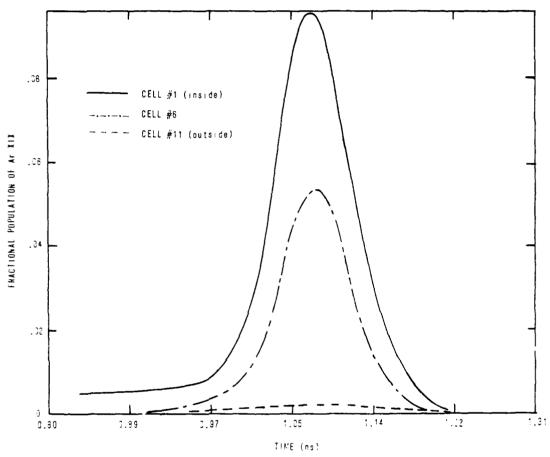


Fig. 6 — Fractional population of Ar XIX vs time

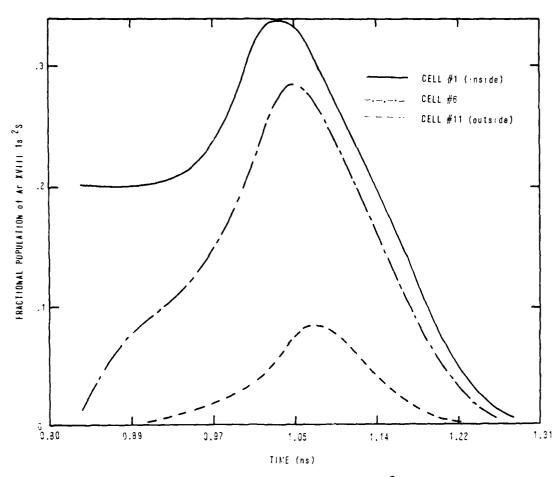


Fig. 7 — Fractional population of Ar XVIII $1s^2S$ vs time

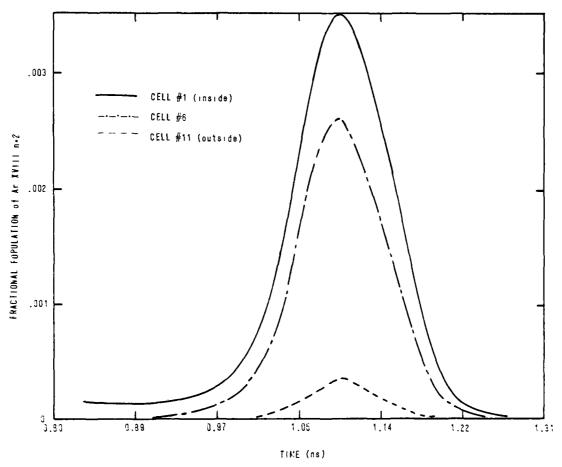


Fig. 8 — Fractional population of Ar XVIII n=2 vs time

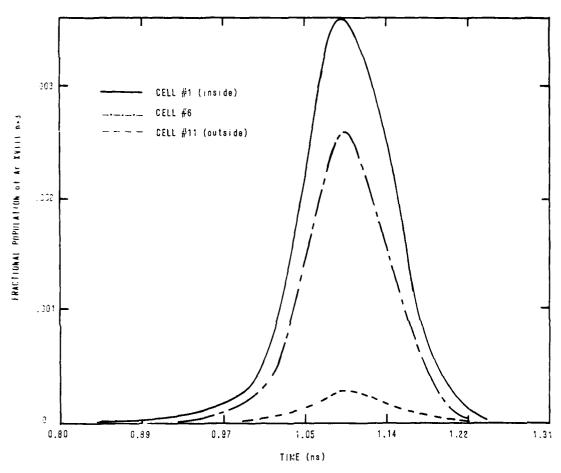


Fig. 9 — Fractional population of Ar XVIII n=3 vs time

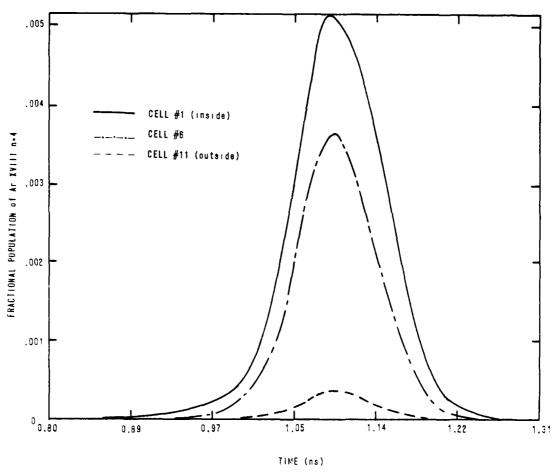


Fig. 10 — Fractional population of Ar XVIII n=4 vs time

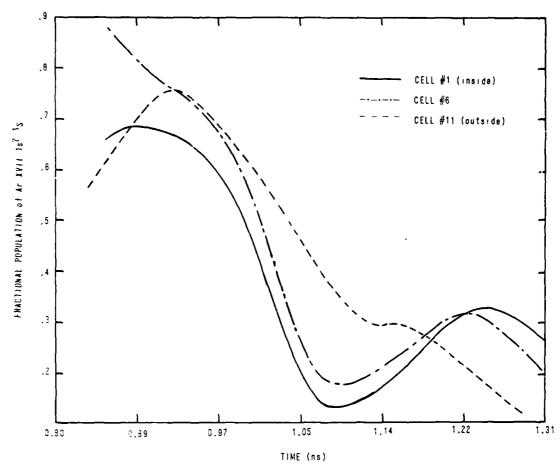


Fig. 11 — Fractional population of Ar XVII 1s² ¹S vs time

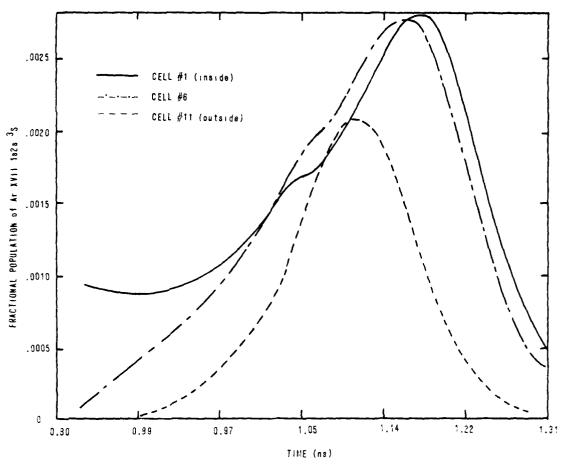


Fig. 12 - Fractional population of Ar XVII 1s2s ³S vs time

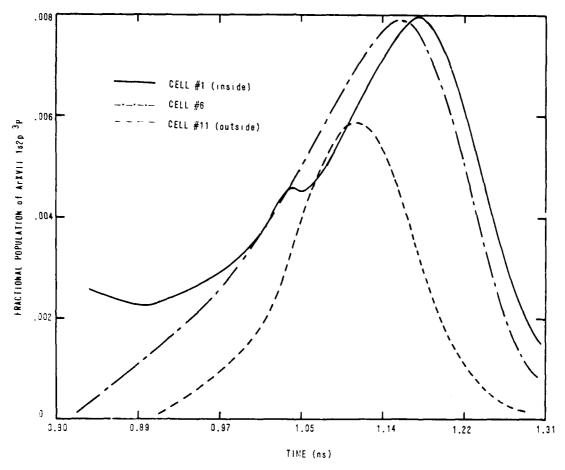


Fig. 13 — Fractional population of Ar XVII 1s2p $^3\mathrm{P}$ vs time

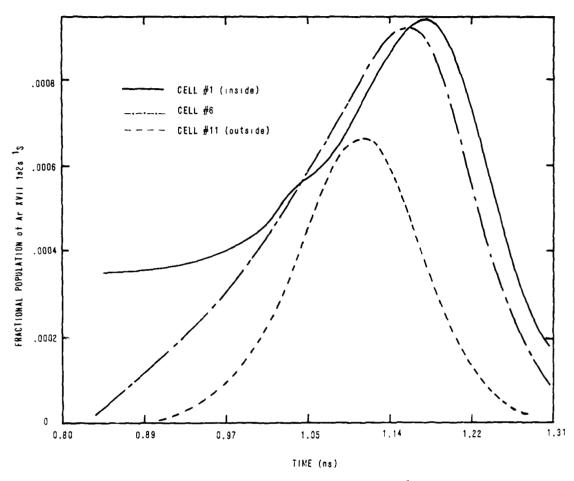


Fig. 14 — Fractional population of A⁻ XVII 1s2s ¹S vs time

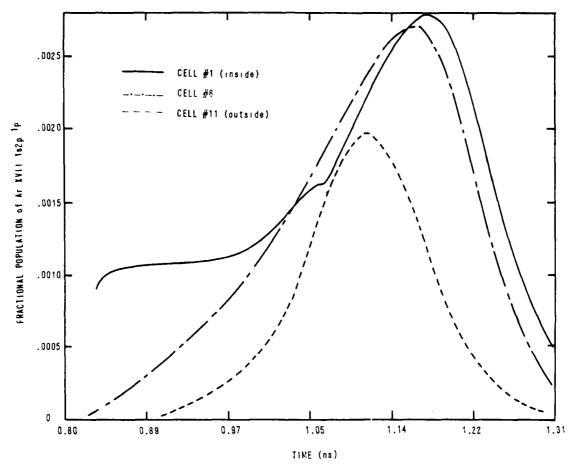


Fig. 15 — Fractional population of Ar XVII 1s2p $^{1}\mathrm{P}$ vs time

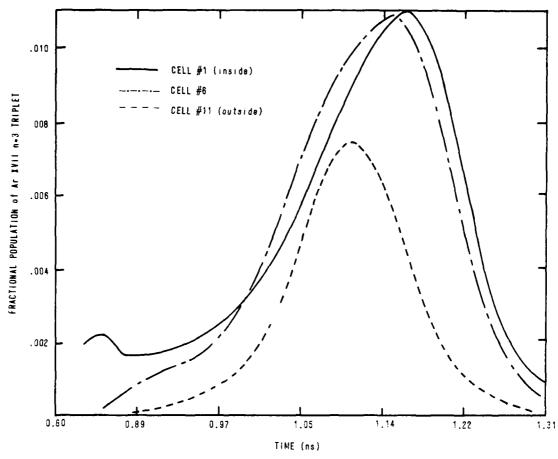


Fig. 16 - Fractional population of Ar XVII n=3 triplet vs time

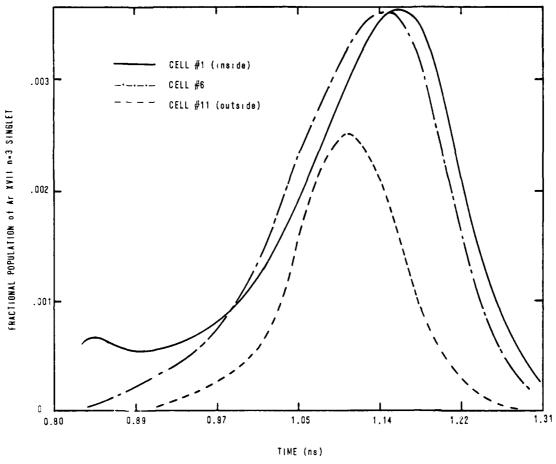


Fig. 17 — Fractional population of Ar XVII n=3 singlet vs time

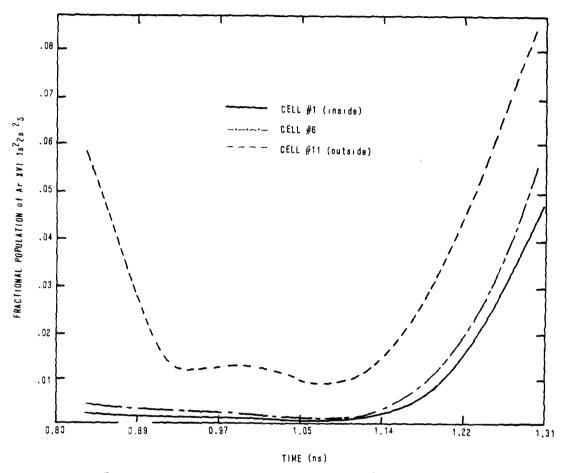


Fig. 18 — Fractional population of Ar XVI 1s²2s ²S vs time

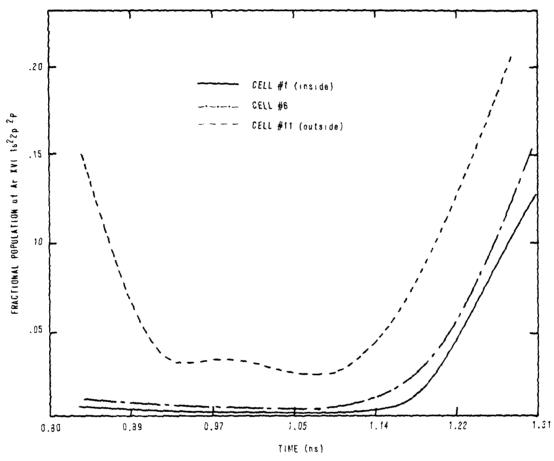


Fig. 19 — Fractional population of Ar XVI 1s 2 2p 2 P vs time

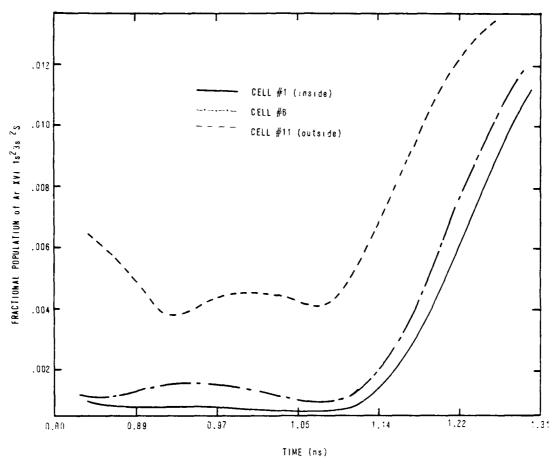


Fig. 20 — Fractional population of Ar XVI $1s^23s$ 2S vs time

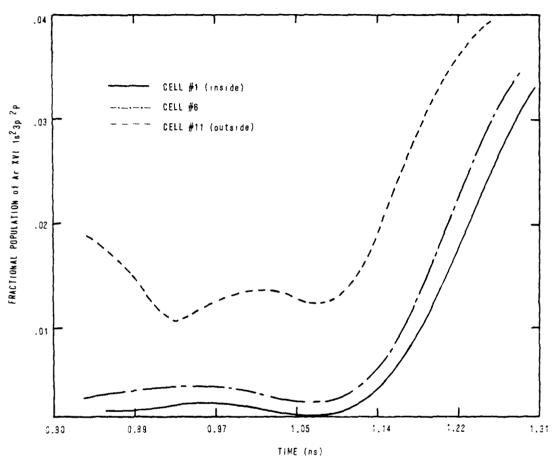


Fig. 21 — Fractional population of Ar XVI 1s 2 3p 2 P vs time

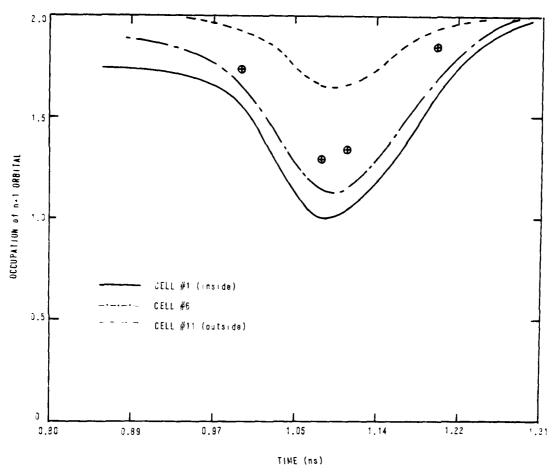


Fig. 22 — Occupation of the n=1 orbital vs time. The points marked Θ were calculated by LASNEX for the inner cell (no. 1).

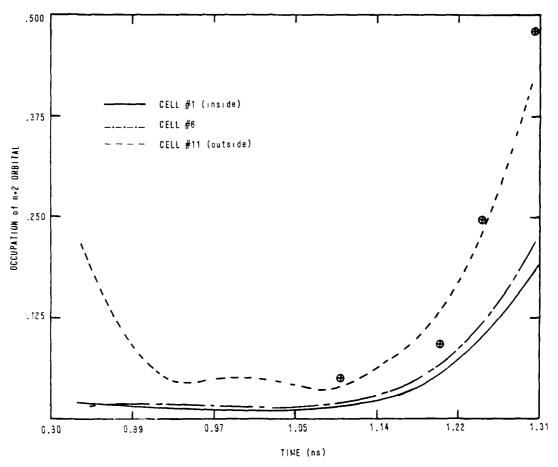


Fig. 23 — Occupation of the n=2 orbital vs time. The points marked ⊕were calculated by LASNEX for the inner cell (no. 1).

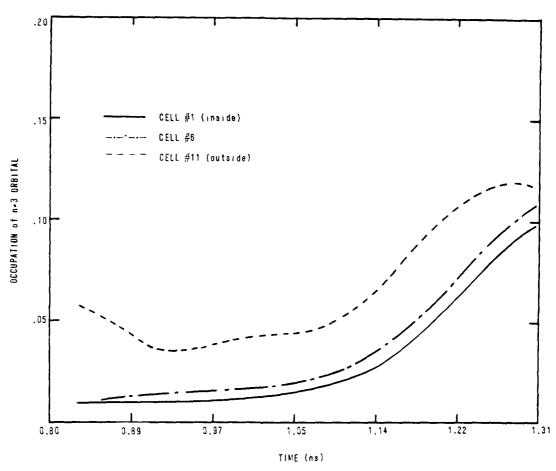


Fig. 24 — Occupation of the n=3 orbital vs time

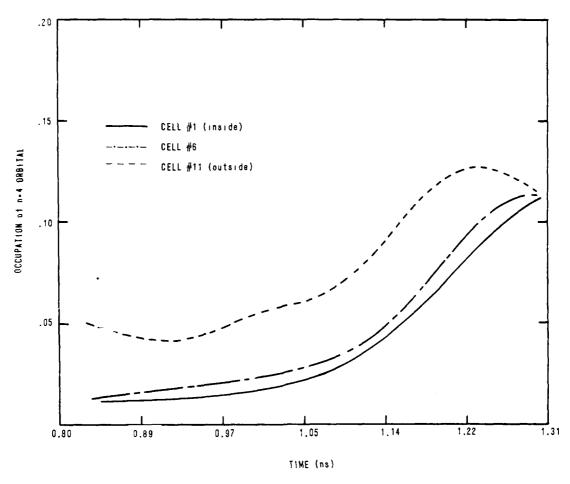


Fig. 25 — Occupation of the n=4 orbital vs time

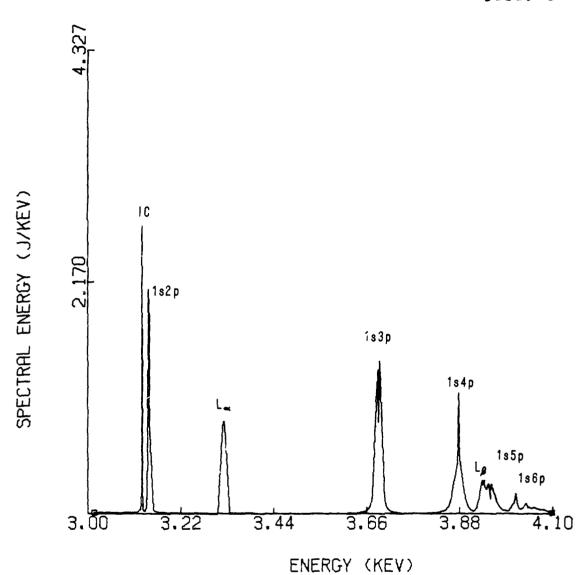


Fig. 26 — Spectrum integrated from 0.8 to 1.06 ns

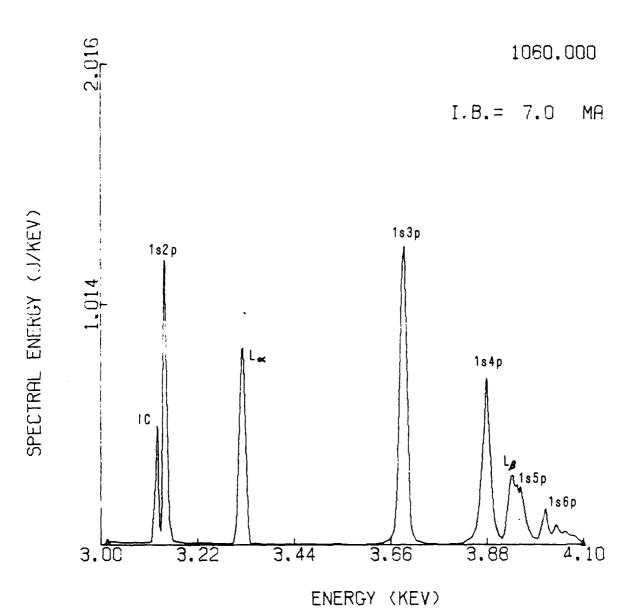


Fig. 27 — Spectrum integrated from 0.8 to 1.06 ns. (Corrected for source and instrumental broadening.)

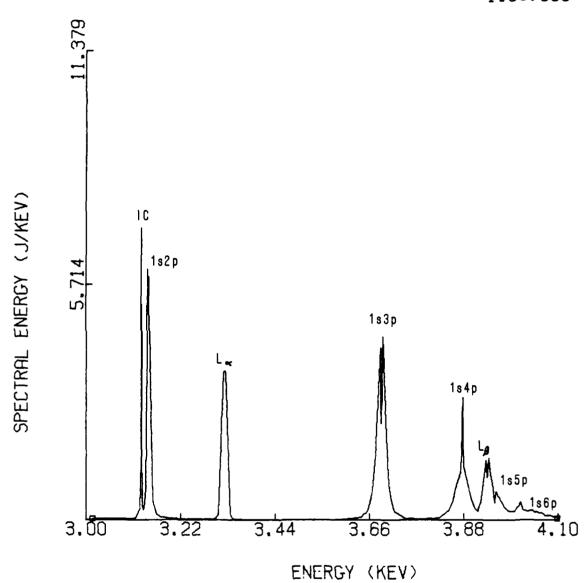


Fig. 28 — Spectrum integrated from 0.8 to 1.18 ns

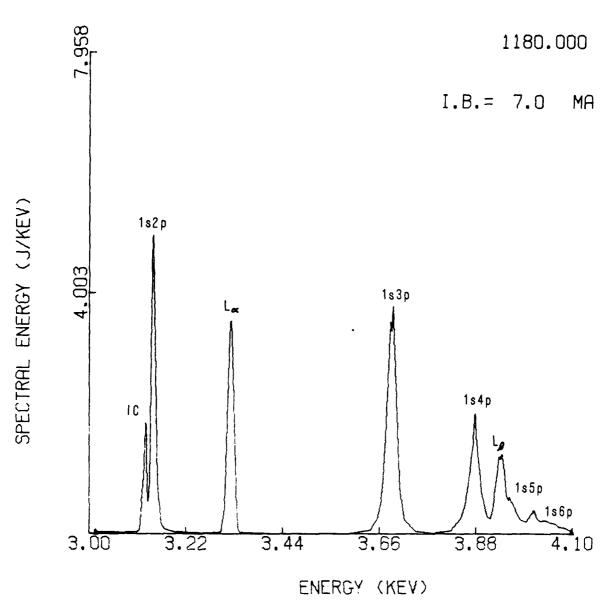


Fig. 29 — Spectrum integrated from 0.8 to 1.18 ns. (Corrected for source and instrumental broadening.)

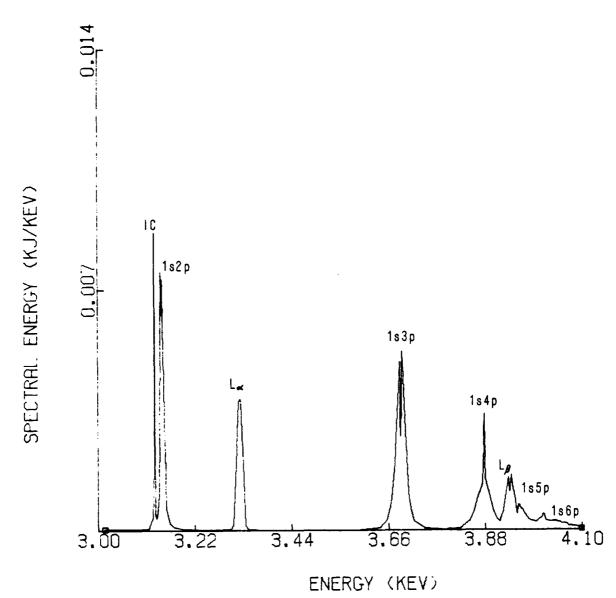


Fig. 30 — Spectrum integrated from 0.8 to 1.3 ns

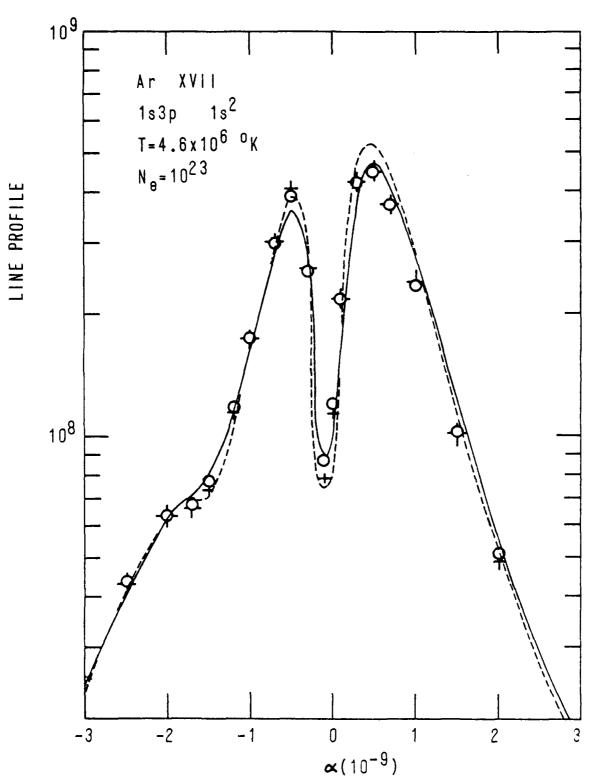


Fig. 31 — Stark profile of Ar XVII 1s3p—1s². The dashed line corresponds to calculations which include the singlet states only. The solid line to calculations which include mixing of singlet and triplet states. The points marked O and + were calculated neglecting the imaginary (shift) part of the electron operator. The points marked + were calculated using an approximation in the real part of the electron broadening.

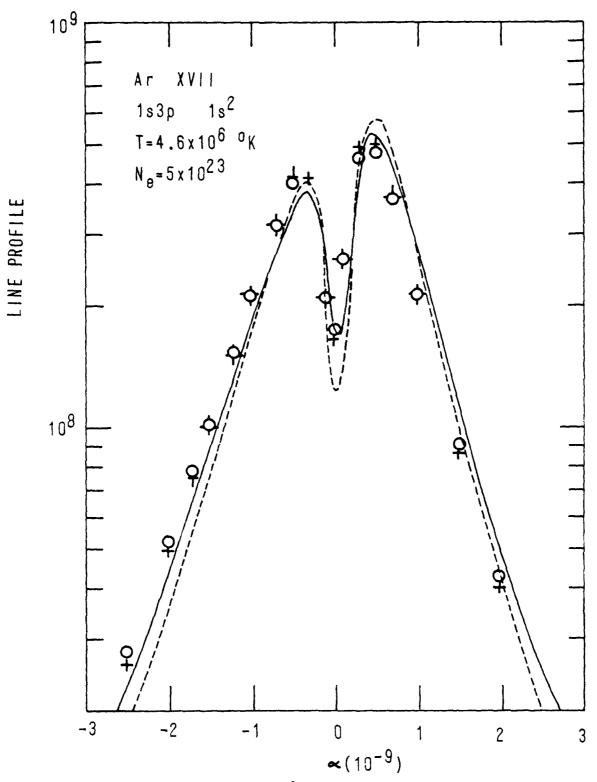


Fig. 32 — Stark profile of Ar XVII $1s3p-1s^2$. The dashed line corresponds to calculations which include the singlet states only. The solid line to calculations which include mixing of singlet and triplet states. The points marked O and + were calculated neglecting the imaginary (shift) part of the electron operator. The points marked + were calculated using an approximation in the real part of the electron broadening.

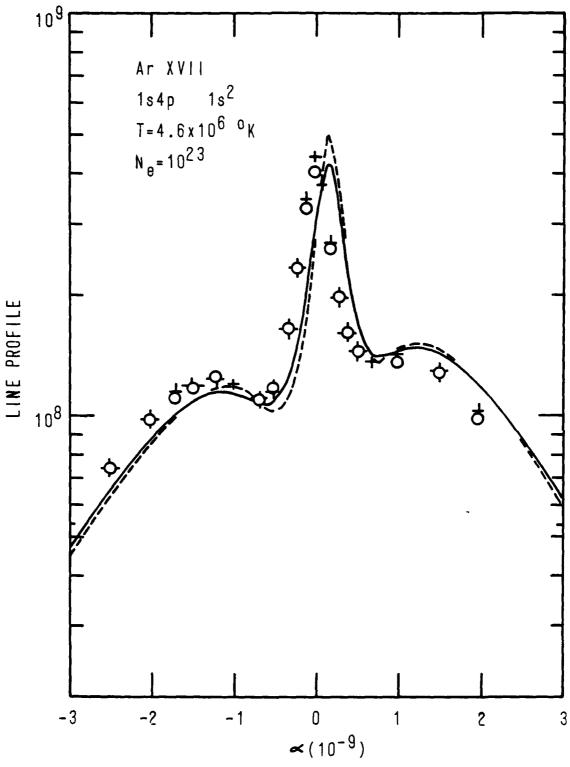


Fig. 33 — Stark profile of Ar XVII 1s4p—1s². The dashed line corresponds to calculations which include the singlet states only. The solid line to calculations which include mixing of singlet and triplet states. The points marked O and + were calculated neglecting the imaginary (shift) part of the electron operator. The points marked + were calculated using an approximation in the real part of the electron broadening.

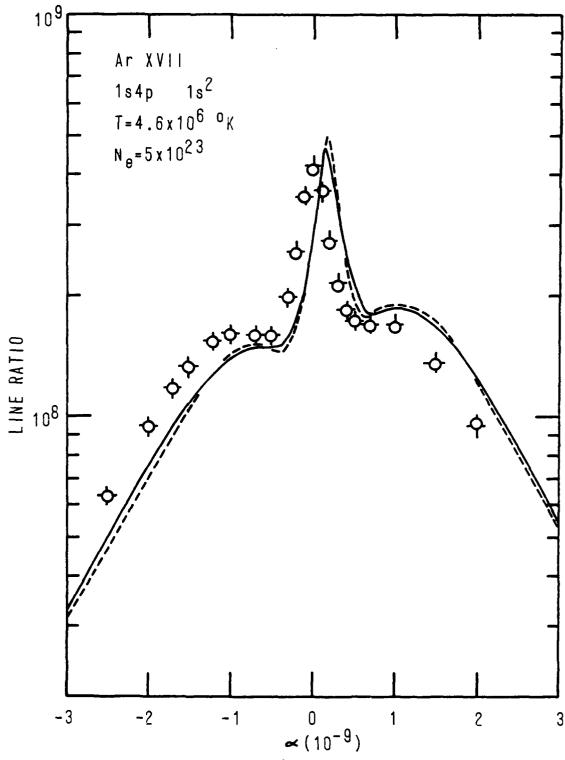


Fig. 34 — Stark profile of Ar XVII 1s4p—1s². The dashed line corresponds to calculations which include the singlet states only. The solid line to calculations which include mixing of singlet and triplet states. The points marked O and + were calculated neglecting the imaginary (shift) part of the electron operator. The points marked + were calculated using an approximation in the real part of the electron broadening.

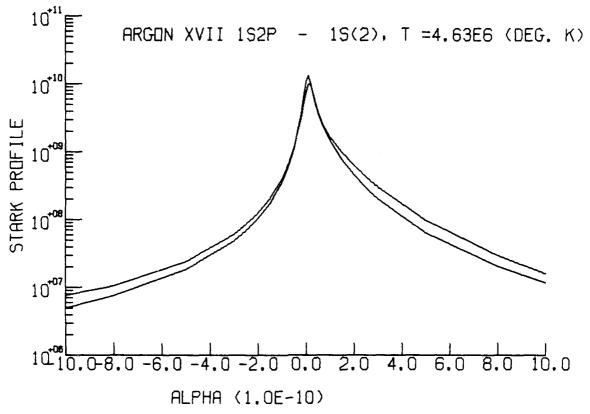


Fig. 35 — Stark profile of Ar XVII 1s2p—1s2

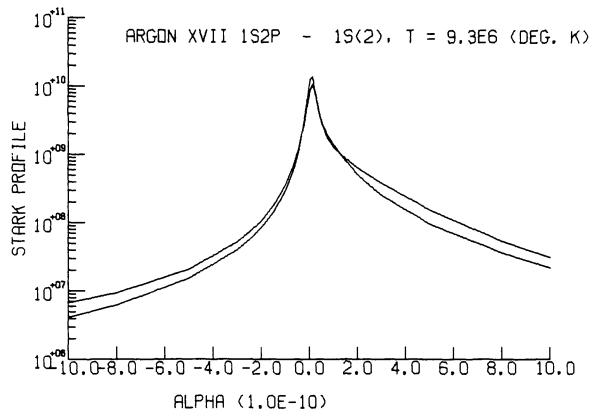


Fig. 36 - Stark profile of Ar XVII 1s2p-1s2

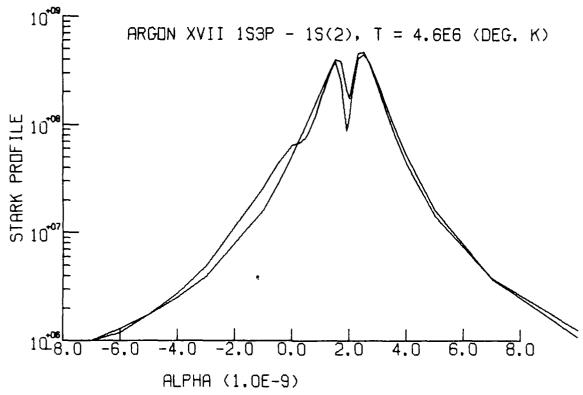


Fig. 37 — Stark profile of Ar XVII 1s3p—1s²

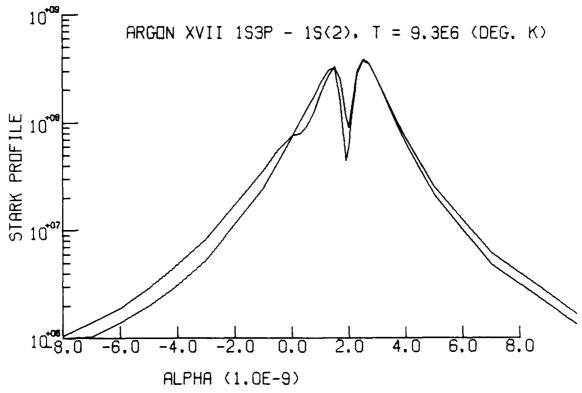
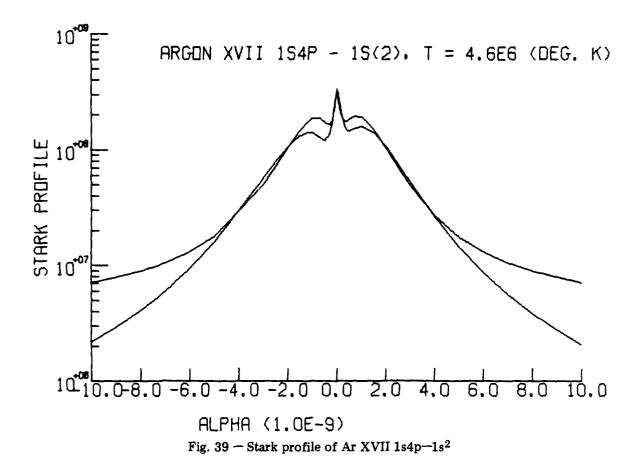
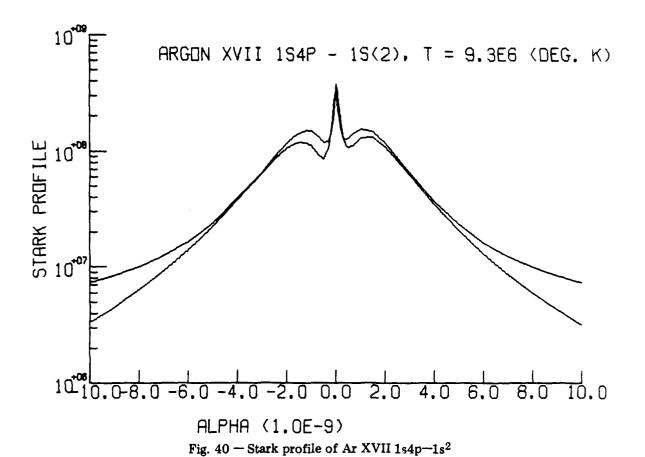


Fig. 38 — Stark profile of Ar XVII 1s3p—1s²





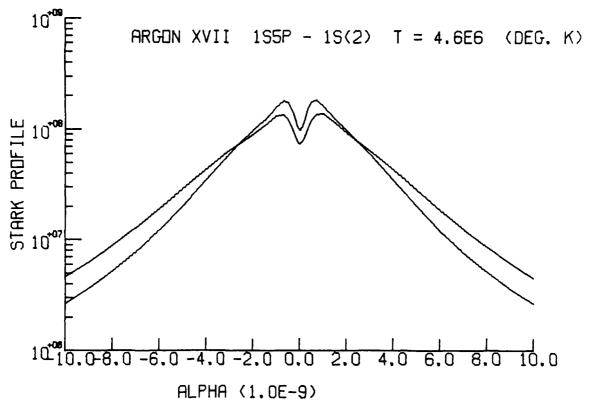


Fig. 41 — Stark profile of Ar XVII 1s5p—1s²

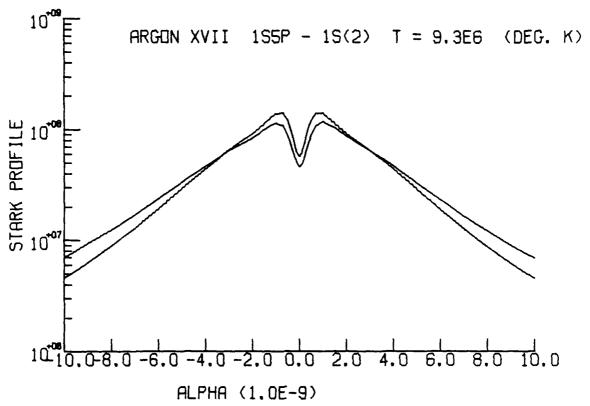


Fig. 42 — Stark profile of Ar XVII 1s5p—1s2

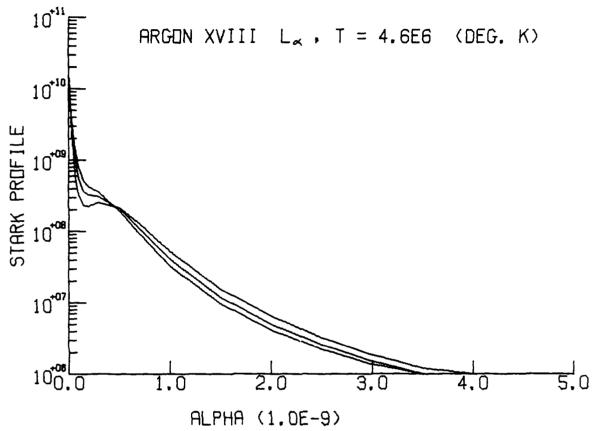
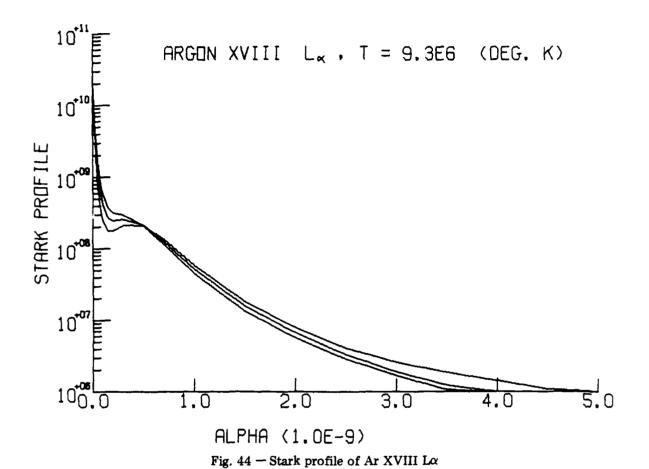
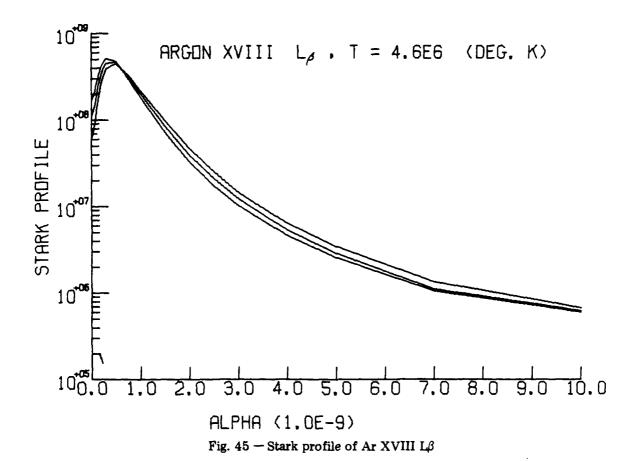
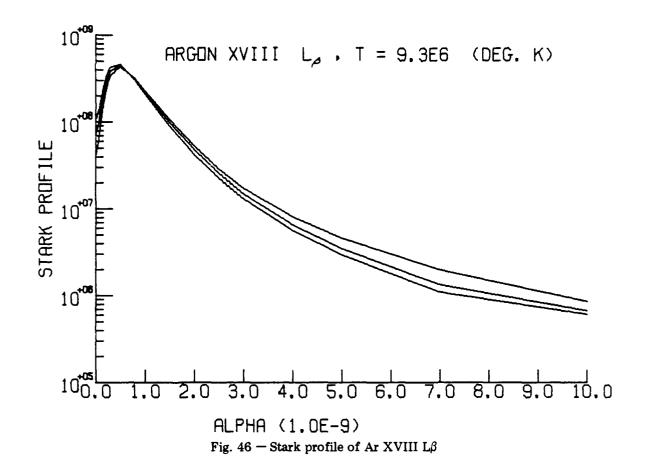


Fig. 43 — Stark profile of Ar XVIII Lα







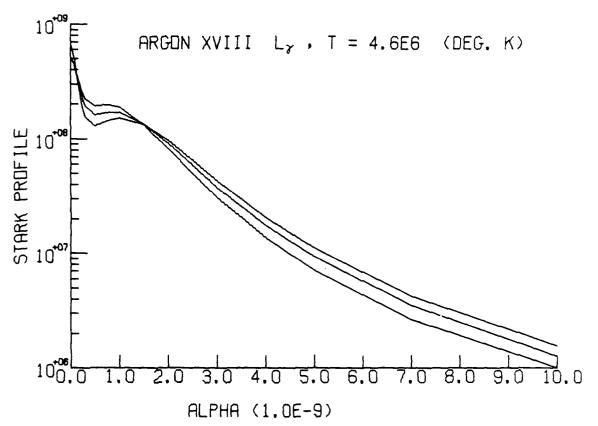
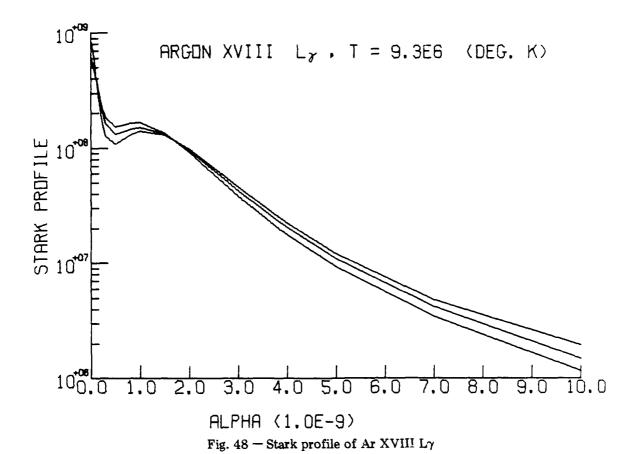


Fig. 47 — Stark profile of Ar XVIII L γ



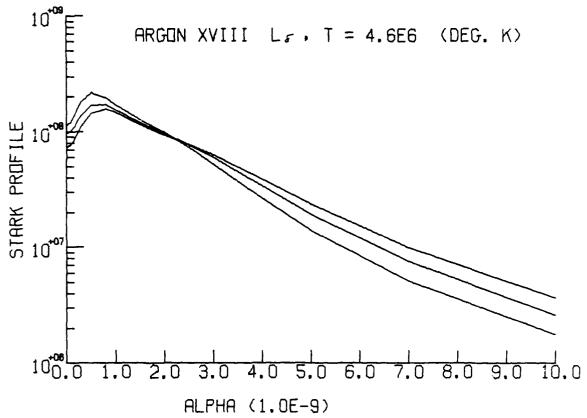
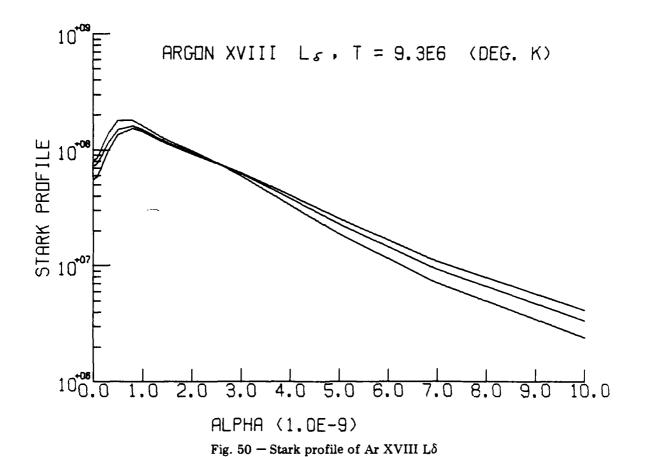


Fig. 49 — Stark profile of Ar XVIII $L\delta$



Ar XXII, n = 3

	'S	'P	,D	³S	³P	³ D
1 S 29694422 -4.58 eV		þ				
1P 29731382 0.00 eV	1		.88421			-46709
¹ D 29729378 -0.25 eV		.88421			46709	
³ S 29654518 -9.52eV					1	
³ P 29697464 -420eV			-,46709)		88421
³ D 29725922 -0.68eV		46709			88421	

Ar XXIII, n = 4

	'S	'P	'D	'F	³S	³P	δ	³F
1 31253221 -1.90eV								
¹ P 31273557 0.00 eV	1		903				.429	
31273143 -0.05 eV		903		0.965		.429		0.259
1 31274163 0.08eV			0.965				0.259	
³ S 31241873 -3.92eV								
³ P 31259573 -1.73 eV			.429				.903	
3 3!27!579 -0.24eV		.429		0.259		.903		-0.965
³ F 31273555 0.00 eV			0.25\$				-G.965	

Table 3 Ar XVII n = 5

	18	lρ	1 _D	٦ _F	١ _G	38	3 _p	3 _D	3 _F	3 _G
1 _S 319 79 581 -0.970 eV		ì								
319 87 403 0.0 eV	1		9097					+4152		
319 87 311 -0.01 eV		9 097		.9 630			4152		26 9 0	
1 _F 319 87 906 +0.06 eV			.9630		.9996			.2 693		0286
16 319 88 300 +0.11 eV				.9996					. 0286	
³ S 319 71 606 - 1.96							1			
3 _p 319 80 726 -0.83			- 4152			1		9097		
³ p 319 86 769 -0.08		.4152		2693			- . 9097		. 963 0	
3 _F 319 87 583 +0.02	3		- 2693		.0286			.9630		.999 6
3 _G 319 ₆ 88 ₁ 279	9			0286					.9996	

Table 4
C (10⁻⁹)

Т	4.6	5x10 ⁶	9.3	x 10 ⁶
N _e	10 ²³	5 x 10 ²³	10 ²³	5 x 10 ²³
Ar XVII 1s2p 1s39 1s4p 1s5p	.11 .24 .43 .67	.12 .27 .49 .76	.09 .20 .36 .56	.11 .23 .41 .64
Ar XVIII L∝ Lβ Lγ Lδ	.08 .18 .32 .50	.09 .21 .37 .57	.07 .15 .27 .42	.08 .17 .31 .48

Table 5 Stark Profiles for

ARGON XVII 152P - 15(2), T =4.63E6 (DEG. K)

$ \begin{array}{c} N_{e} = & 1.00E \ 23 & 5.90E \ 23 \\ \hline -1.00E-09 & 4.93E \ 06 & 7.64E \ 06 \\ -8.00E-10 & 7.58E \ 06 & 1.07E \ 07 \\ -5.00E-10 & 1.86E \ 07 & 2.42E \ 07 \\ -3.00E-10 & 4.89E \ 07 & 6.09E \ 07 \\ -2.50E-10 & 6.87E \ 07 & 8.45E \ 07 \\ -2.00E-10 & 1.04E \ 08 & 1.25E \ 08 \\ -1.50E-10 & 1.75E \ 08 & 2.07E \ 08 \\ -1.50E-10 & 3.57E \ 08 & 4.07E \ 08 \\ -7.00E-11 & 6.53E \ 08 & 7.12E \ 08 \\ -7.00E-11 & 3.63E \ 09 & 3.14E \ J9 \\ -1.00E-11 & 6.27E \ 09 & 4.82E \ 09 \\ 0.00E-01 & 1.33E \ 10 & 9.93E \ 09 \\ 1.00E-11 & 3.57E \ 07 & 3.81E \ 09 \\ 7.00E-11 & 3.57E \ 07 & 3.81E \ 09 \\ 7.00E-11 & 2.37E \ 07 & 3.81E \ 09 \\ 1.50E-10 & 7.73E \ 08 & 9.78E \ 08 \\ 2.00E-10 & 4.56E \ 08 & 6.31E \ 08 \\ 2.50E-10 & 2.95E \ 08 & 4.32E \ 08 \\ \hline \end{array} $			
-8.00E-10	\propto $N_e =$	1.00E 23	5.00E 23
-8.00E-10	-1.00E-09	4.93E 06	7.64E 06
-5.00E-10	-8.00E-10	7.58E 06	1.07E 97
-3.00E-10	-5.00E-10		
-2.50E-10			
-2.00E-10			
-1.50E-10			
-1.00E-10		. •	
-7.00E-11 6.53E 08 7.12E 08 -5.00E-11 1.11E 09 1.15E 09 -2.00E-11 3.63E 09 3.14E 09 -1.00E-11 6.27E 09 4.82E 09 0.00E 00 1.08E 10 7.42E 09 1.00E-11 1.33E 10 9.93E 09 2.00E-11 9.88E 09 9.55E 09 5.00E-11 3.57E 09 3.81E 09 7.00E-11 2.37E 09 2.51E 09 1.00E-10 1.46E 09 1.65E 09 1.50E-10 7.73E 08 9.78E 08 2.00E-10 4.56E 08 6.31E 08			_
-5.00E-11 1.11E 09 1.15E 09 -2.00E-11 3.63E 09 3.14E J9 -1.00E-11 6.27E 09 4.82E 09 0.00E 00 1.08E 10 7.42E 09 1.00E-11 1.33E 10 9.93E 09 2.00E-11 9.88E 09 9.55E 09 5.00E-11 3.57E 09 3.81E 09 7.00E-11 2.37E 09 2.51E J9 1.00E-10 1.46E 09 1.65E J9 1.50E-10 7.73E 08 9.78E 08 2.00E-10 4.56E 08 6.31E 08			
-2.00E-11 3.63E 09 3.14E J9 -1.00E-11 6.27E 09 4.82E 09 0.00E 00 1.08E 10 7.42E 09 1.00E-11 1.33E 10 9.93E 09 2.00E-11 9.88E 09 9.55E 09 5.00E-11 3.57E 09 3.81E 09 7.00E-11 2.37E 09 2.51E D9 1.00E-10 1.46E 09 1.65E J9 1.50E-10 7.73E 08 9.78E 08 2.00E-10 4.56E 08 6.31E 08			
-1.00E-11 6.27E 09 4.82E 09 0.00E 00 1.08E 10 7.42E 09 1.00E-11 1.33E 10 9.93E 09 2.00E-11 9.88E 09 9.55E 09 5.00E-11 3.57E 09 3.81E 09 7.00E-11 2.37E 09 2.51E 09 1.50E-10 1.46E 09 1.65E 09 1.50E-10 7.73E 08 9.78E 08 2.00E-10 4.56E 08 6.31E 08		• • •	
0.00E 00 1.08E 10 7.42E 09 1.00E-11 1.33E 10 9.93E 09 2.00E-11 9.88E 09 9.55E 09 5.00E-11 3.57E 09 3.81E 09 7.00E-11 2.37E 09 2.51E 09 1.00E-10 1.46E 09 1.65E 09 1.50E-10 7.73E 08 9.78E 08 2.00E-10 4.56E 08 6.31E 08			
1.00E-11			
2.00E-11			
5.00E-11 3.57E 07 3.81E 09 7.00E-11 2.37E 09 2.51E 09 1.00E-10 1.46E 09 1.65E 09 1.50E-10 7.73E 08 9.78E 08 2.00E-10 4.56E 08 6.31E 08	<u>-</u>		
7.00E-11 2.37E 09 2.51E 09 1.00E-10 1.46E 09 1.65E 09 1.50E-10 7.73E 08 9.78E 08 2.00E-10 4.56E 08 6.31E 08		-	
1.00E-10			
1.50E-10 7.73E 98 9.78E 98 2.00E-10 4.56E 08 6.31E 08		•	
2.00E-10 4.56E 08 6.31E 08			
			•
CARLO SA CARLOS ASSESSED AND CONTRACTOR OF CONTRACTOR C			
3.00E=10 2.01E 08 3.05E 08		. •	
5.00E-10 6.35E 07 9.83E 07			
8.00E-10 2.07E 07 2.96E 07		7	
1.00E-09 1.19E 07 1.62E 07			

Table 6
Stark Profiles for

ARGON XVII 1820 - 18(2), T = 9.3E6 (DEG. K)

× N _e =	1.00E	23	5.00E	23
-1.09E-09	4.10E	06	6.76E	96
-8.00E-10	385°9		9.32E	06
-5.00E-10	1.54E		2.09E	07
-3.00E-10	4.03E		5.25E	07
-2.50E-10	5.67E	07	7.308	07
-2.00E-10	8.58E	07	1.09E	98
-1.50E-10	1.46E	08	1.825	98 98
-1.00E-10	3.03E	98	3.67E	30
-7.00E-11	5.66E	08	6.676	98
-5.00E-11	9.93E	08	1.11E	09
		93		09
-2.00E-11	3.64E		3.36E	
-1.00E-11	6.86E	0.3	5.44E	09
0.00E 00	1.288	10	8.67E	19
1.00E-11	1.38E	10	1.07E	10
2.00E-11	8.38E	0.0	8,61E	39
5.00E-11	2.86E	09	2.78E	0.9
7.00E-11	2.01E	0.9	1.82E	29
1.00E-10	1.35E	09	1.26E	09
1.50E-10	7.92E	98	8.65E	ባዶ
2.00E-10	5.04E	ტვ	6.40E	0.8
2.50E-10	3.51E	08	4.87E	9.6
3.00E-10	2.53E	08	3.77E	0 &
5.00E-10	9.55E	07	1.54E	0.8
8.00E-10	3.66E	97	5.44E	37
1.00E-09	2.19E	07	3.10E	07

Table 7
Stark Profiles for

ARGON XVII 183P - 18(2), T = 4.6E6 (DEG. K)

N _e =	1.008 23	5.00E 23
_		
-1.00E-08	6.76E 05	7.97E 05
-9.00E-09	8.80E 05	1.00E 06
-8.00E-03	1.19E 06	1.30E 06
-7.00E-09	1.74E 06	1.75E 06
-6.00E-03	2.76E 06	2.51E 06
-5.00E-09	4.93E 06	3.94E 96
-3.00E-09	2.63E 07	1.63E 07
-2.50E-09	4.36E 07	2.78E 07
-2.00E-09	6.38E 07	5.17E 07
-1.70E-09	6.88E 07	7.75E 07
-1.50E-09	7.73E 07	1.02E 08
-1,20E-09	1.19E 08	1.54E 08
-1.00E-09	1.76E 08	2.06E 08
-7.00E-10	2.97E 08	3.14E 08
-5.00E-10	3.89E 08	4.00E 08
-3.00E-10	2.52E 08	3.89E 08
-1.00E-10	8.76E 07	2.07E 08
0.00E 00	1.20E 08	1.76E 08
1.09E-10	2.12E 08	2.56E 98
3.00E=10	4.11E 08	4.58E 08
5.00E-10	4.48E 08	4.72E 08
7.00E-10	3.74E 08	3.65E 08
1.00E-09	2.35E 08	2.16E 18
1.50E=09	1.04E 08	9.05E 07
2.00E=09		•
3.00E-09	5.10E 07	·
	1.60E 07	1.418 07
5.00E-09	3.68E 06	3.73F 06
8.00E-09	1.09E 06	1.27E 06

Table 8
Stark Profiles for

ARGON XVII 183P - 18(2), T = 9.3E4 (DEG. K)

\propto $N_e =$	1.00E 23	5.00E 23
-1.00E-08	1.05E 06	7.97E 05
-9.00E-09	1.39E 06	1.03E 06
-8.00E-09	1.89E 06	1.40E 06
-7.00E-09	2.94E 06	2.00E 06
-6.00E-09	4.83E 06	3.12E 06
-5.00E-09	8.50E 06	5.35E 06
-3.00E-09	3.60E 07	2.50E 07
-2.508-09	5.56E 07	4.23E 07
-2.0nE-09	7.55E 07	7.42E 07
-1.70E-09	8.02E 07	1.04E 08
-1.5nE-09	9.11E 07	1.30E 08
-1,20E-09	1,33E 08	1.80E 08
-1.00E-09	1.87E 08	2.32E 08
-7.00E-10	2.76E 08	3.08E 08
-5,00E-10	3.32E 08	3.27E 08
-3.00E-10	1.58E 08	2.58E 08
-1.00E-10	4.46E 07	1.14E 08
0.00E 00	6.11E 07	9.04E 07
1.00E-10	1.17E 08	1.47E 08
3.00E-10	2.88E 93	3.08E 08
5.00E-10	3.80E 08	3.92E 08
7.00E-10	3.58E 08	3.60E 08
1.00E-09	2.52E 98	2.51E 08
1.50E-09	1.29E 08	1.23E 08
2.00E-09	7.15E 07	6.36E ^7
3.00E-09	2.54E 07	2.13E
5.00E-09	6.17E 06	4.0
8.0nE-09	1.68E 06	1 L 06

Table 9
Stark Profiles for

ARGON XVII 1S4P = 1S(2), T = 4.6E6 (DEG. K)

\propto $N_e =$	1.00E 23	5.00E 23
7 /6		200.5 53
-1.00E-08 -9.00E-09	2.10E 06	1.65E 06
-8.00E-09	2.83E 06	2.13E 06
-7.09E-09	3.97E 06 5.89E 06	2.88E 06
-6.00E-09		4.11E 06
+5.00E=09	9.31E 06 1.58E 07	6.31E 06
-3.07E-09	5.49E 07	1.06E 07
-2.50E-09	7.51E 07	4.24E 07 6.30E 07
-2.01E-09	9.88E 07	6.30E 07 9.50E 07
-1.70E-09	1.12E 95	1.18E 08
-1.50E-09	1.18E 08	1.34E 08
=1.20E=09	1.22E 08	1.54E 08
-1.00E-09	1.19E 08	1.62E 08
-1.00E-09 -7.00E-10 -5.00E-10	1.12E 08	1.60E 08
-3.00E-10	1.18E 08	1.60E 08
-2.00E-10	1.68E 08	80 300.5
-1.00E-10	2.33E 08 3.34E 08	3.60E 08
0.00E 00	4.08E 08	3.53E 08
1.09E-10	3.61E 98	4.15E 08 3.64E 08
2.00E-10	2.66E 08	2.74E 08
3.00E-10	1.99E 08	2.15E 08
4.00E-10	1.64E 08	1.85E 08
5.00E-10	1.46E 08 1.37E 08	1.74E 08
7.00E-10	1.37E 08	1.71E 08
1.00E-09 1.50E-09	1.39E 03	1.69E 08
2.00E-09	1.29E 08	1.36E J8
3.00E-09	1.02E ns	9.46E 07
4.00E-09	5.29E 07 2.70E 07	4.15E 07
5.00E-09	1.48E 07	1.95E 07
6.00E-09	8.76E 96	1.04E 07 6.20E 06
7.00E-09	5.60E 06	6.20E 06 4.06E 06
8.00E-09	3.81E 06	2.85E 06
9.00E-09	2.73E 06	2.12E 06
1.00E-08	2.04E 06	1.64E 06

Table 10 Stark Profiles for

ARGON	XVII	154P	•	15(2),	7 =	9.3E6 (DEG. K)	
	<u>«</u>	N _e =		1.00E	23	5.008	23	
-9 -8 -7 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1	00000000000000000000000000000000000000	08999999999999999999999999999999999999		1.00 2439EEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEE	2 000000000000000000000000000000000000	2.00 185EEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEE	2 000000000000000000000000000000000000	
4 5 7 1 1 2 3 4 5 6 7 8 9	.00E0	10 10 10 09 09 09 09 09 09		1.28E 1.01E 1.01E 1.08E 1.08E 1.08E 1.08E 1.08E 1.08E 1.09E	008 008 008 007 007 007 007 006 006	1.39E 1.29E 1.19E 1.27E 1.24E 1.02E 5.56E 2.91E 1.61E 9.56E 4.11E 9.59E 4.11E	088 088 088 087 077 066 066 066	

Table 11 Stark Profiles for

-	15(2)	T	=	4.6E6	(DEG.	K)
	1.00E	23		5.00E	23	
	4.60E	06		2.658	06	
		06			06	
					06	
					26	
	1.91E				27	
					0.7	
					_	
	1.09E					
	1.23E					
				1.59E		
	1.35E			1.80E		
	1.23E				0.8	
					08	
					0.8	
					9.0	
					08	
		_			9.0	
					80	
					80	
	1.15E				08	
	9.36E					
					06	
		96			06	
		00			06	
	4.53E	06		2.64E	06	
		E EEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEEE	1.0000777777777777777777777777777777777	23 6666777777777777777777777777777777777	1.00E 23 5.00E 4.60E 06 3.63E 8.83E 06 5.17E 1.28E 07 1.22E 2.90E 07 6.03E 7.63E 07 7.79E 1.01E 08 1.22E 1.09E 08 1.43E 1.09E 08 1.580E 1.32E 08 1.580E 1.32E 08 1.580E 1.32E 08 1.580E 1.32E 08 1.64E 1.32E 07 1.06E 8.84E 07 1.06E 8.84E 07 1.06E 8.89E 07 1.06E 8.89E 07 1.06E 8.89E 07 1.06E 8.89E 07 1.64E 1.38E 08 1.63E 1.38E 07 1.21E 7.69E 1.25E 07 7.69E 1.25E 07 7.69E 3.61E	1.00E 23 5.00E 23 4.60E 06 2.65E 06 8.83E 06 5.17E 06 1.28E 07 7.76E 06 1.29E 07 1.22E 07 2.90E 07 2.03E 07 7.63E 07 7.77E 07 9.02E 07 9.79E 07 1.01E 08 1.22E 08 1.09E 08 1.43E 08 1.23E 08 1.43E 08 1.23E 08 1.45E 08 1.32E 08 1.46E 08 1.32E 08 1.76E 08 1.32E 08 1.76E 08 1.32E 08 1.76E 08 1.32E 08 1.65E 08 1.33E 08 1.65E 08 1.35E 07 1.06E 08 1.46E 07 1.05E 08 1.36E 07 1.66E 08 1.37E 08 1.63E 08 1.39E 07 1.64E 07 1.48E 07 1.22E 08 1.35E 07 1.64E 08 1.35E 08 1.63E 08 1.35E 07 1.69E 06 1.35E 07 7.69E 06

Table 12 Stark Profiles for

ARGON XVII 1	35P -	15(2)	T =	9.3E6	(DEG.	K)
X N	e =	1.00E	23	5.00E	23	
-1.00E-08	3	7.06E	06	4.58E	06	
-9,00E-09		9.27E	06	6.28E	96	
-8.00E-09		1.24E	07	8.88E	06	
-7.00E-09		1.70E	07	1.29E	·)7	
-6.00E-09		2.37E	07	1.93E	07	
-5.00E-09		3,37E	07	2.94E	07	
-3.00E-09		6.43E	07	6.52E	07	
-2.50E-09)	7.34E	07	7.74E	07	
-2.00E-09		8.39E	97	9.17E	07	
-1.70E-09)	9.22E	07	1.03E	9.0	
-1.50E-09)	9.90E	07	1.12E	08	
-1.20E-09)	1.10E	08	1.29E	98	
-1.09E-09)	1.14E	98	1.39E	98	
-7,00E-10)	1.08E	60	1.40E	08	
-5.00E-10		9.03E	07	1.22E	0.8	
-3.00E-10)	6.75E	07	8.99E	07	
-2.00E-10		5.74E	97	7.40E	07	
-1,00E-10)	5.00E	97	6.21E	07	
0.00E 00		4.65E	07	5.71E	07	
1.00E-10	1	4.79E	07	6.09E	07	
2,00E-10	;	5.41E	07	7.24E	37	
3.00E-10	t	6.39E	07	8.84E	77	
4.00E-10	1	7.59E	07	1.06E	9.0	
5.00E-10	1	8.83E	07	1.21E	9.0	
7.00E-10		1.09E	იგ	1.41E	08	
1.00E-09		1.19E	ე8	1.41E	36	
1.50E-09		1.04E	98	1.14E	98	
2.00E=09		8.77E	07	9.30E	07	
3.00E-09		6.54E	07	6.54E	07	
4.00E=03		4.75E	07	4.45E	07	
5.00E-09		3.34E	97	2.92E	97	
6.00E-09		2.34E	07	1.91E	07	
7.00E-09		1.67E	07	1.28E	07	
8.00E-09		1.22E	97	8.81E	06	
9.01E-09		9.13E	06	6.24E	36	
1.01E-08		6.96E	06	4.55E	96	

Table 13 Stark Profiles for

ARGON XV	III LX	, 7 =	4.6E6	(DEG	. K)	
$N_e =$	1.00E	55	1.00E	23	5.00E	23
0.00E 00	1.69E	10	9.81E	09	7.02E	09
3.00E-12	1.60E	10	9.62E	() ?	6.958	03
1.00E-11	1.01E	19	8.05E	39	6.34E	09
3.00E-11	2.42E	09	3.34E	09	3.63E	Ç9
5.00E-11	9.92E	98	1.59E	09	2.01F	C è
7.0JE-11	5.55E	ე8	9.31E	08	1.26E	0.9
1.00E-10	3.27E	08	5.53E	0.8	7.76E	9.0
1.50E-10	2.315	08	3.67E	08	5.06E	9.0
2.00E-10	2.24E	ეგ	3.24E	0.5	4.22E	36
3.00E-10	2.50E	08	3.05E	96	3.47E	9.0
5.00E-10	2.13E	0.5	2.08E	9 E	1.948	υē
7.00E-10	1.27E	08	1.09E	9 <u>8</u>	9.15E	07
1.00E-09	5.14E	07	4.06E	0 <u>7</u>	3.24E	07
1.50E-09	1.54E	97	1.19E	97	9.55E	96
2.00E-09	6.54E	06	5.01E	n 6	4.13E	06
2.506-09	3.21E	06	2.57E	06	2.21E	06
3.00E-09	1.86E	06	1.52E	06	1.37E	16
3.50E-09	1.21E	06	9.73E	95	9.32E	05
4.00E-09	8.39E	05	6.56E	05	6.71E	25
4.50E-09	6.12E	05	4.67E	05	5.04E) S
5.00E-09	4.75E	05	3.50E	15	3.92E	05

Table 14 Stark Profiles for

ARGON XVI	II La	. † =	9.306	(DEG.	K1	
· -	• •			(,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	, ,,	
\propto N _e =	1.00E	55	1.00E	23	5.01E	23
0.00E 00	2.27E	10	1.27E	1.0	9.00E	9
3.06E=12	2.04E	1 0	1.24E	10	8.85E	7,9
1.00E-11	1.02E	10	9.28E	09	7.60E	74
3.00E-11	1.91E	00	2.91E	0 a	3.418	05
5.00E-11	7.50E	28	1.258	09	1.67E	0.5
		_			-	
7.00E-11	4.15E	98	7.08E	80	9.84E	υē
1.00E-10	2.44E	08	4.10E	98	5.78E	3.0
1.50E-10	1.78E	უ8	2.71E	9 8	3.70E	J G
2.00E-10	1.79E	98	2.46E	98	3.18E	U G
3.00E-10	2.16E	98	2.56E	9月	2.05E	2.6
5.00E-10	5.09E	ეჩ	2.12E	() B	2.198	ŋ ē
7.00E-10	1.36E	08	1.26E	90	1.15E	Λ.A
1.00E-09	5.83E	07	5.14E	97	4 44E	υ7
1.50E-09	1.80E	_	1.56E	97		_
		07			1.33E	07
2.008-09	7.84E	06	0.65E	06	5.65E	06
2.508-09	4.06E	06	3.31E	36	3.88E	06
3.0rE-09	2.585	16	1.91E	26	1.67E	76
3.50E-09	1.87E	06	1.24E	06	1.06E	06
4.00E-09	1.41E	90	8.48E	05	7.07E	15
4.50E-09	1.09E	06	6.15E	15	5 nnE	ςĒ
5.00E-07	8.61E	05	4.75E	US	3.75E	05

Table 15 Stark Profiles for

ARGEN X	VIII Lp. T	= 4.6E6 (D	EG. K)
N _e =	1.00E 22	1.00E 23	5.01E 23
0.00E 00	6.21E 07	1.15E 08	1.738 08
1.00E-11	6.30E 07	1.16E 08	1.74E 08
3.00E-11	6.93E 07	1.23E 08	1.83E 08
5.00E-11	8.12E 07	1.37E 08	1.98E 08
7.00E-11	9.83E 07	1.57E 08	3.208 08
1.00E-10	1.29E 98	1.93E 08	2.635 08
1.20E-10	1.53E 08	2.29E 08	2.942 08
1.50E-10	1.93E 08	2,64E 08	3.41E 08
1.70E-10	2.21E 08	2.94E 08	3.72E 08
2.00E-10	2.64E 18	3.38E 08	4.16E 08
2.50E-10	3.33E 08	4.04E UB	4.768 08
3.00E-10	3.90E 08	4.53E 00	5.14E 08
5.00E-10	4.57E 08	4.70E 08	4.76E 08
8.00E-10	3.12E 08	2.95E 08	2.75E ne
1.00E-09	2.20E 08	5.03E 08	1.83E 08
1.50E-09	9.82E 07	8.50E 07	7.23E 07
2.00E-09	4.70E 07	3.94E 07	3.28E 07
2.50E-09	2.50E 07	2.09E 97	1.73E 07
3.00E-09	1.46E 07	1.23E 07	1.038 07
4.00E-09	6.415 06	5.30E 06	4.65E 06
5.00E-09	3.45E 00	2.85E 16	2.55E 06
7.00E-09	1.35E 06	1.11E 06	1.05E 06
1.00E-08	6.72E 05	6.24E 05	6.05E 05

Table 16 Stark Profiles for

	ARGON	XAIII	، م	• T	=	9.3E6	(DE	G. K)	
×	N _e =	1.0	0E 2	2	1	.noE	23	5.nnE	23
0.00	E 00	4.1	5E 0	7	7	.39E	ა7	1.085	30
1.00		4.2		7		47E	07	1.075	9.0
3.00		4.7		7		.06E	07	1.158	0.8
5.00	E-11	5.8	5E 9	7	9	.20E	77	1.28E	9.0
7.00	E=11	7.2		7	1	.08E	0.8	1.46E	90
1.00	E-10	9.8	7E 0	7	1	.38E	90	1.79E	90
1.20		1.2		8		.60E	9.0	2.04E	90
1.50		1.5		8		.98E	98	2.45E	08
1.70	E-10	1.8		B	2	.24E	30	2.72E	9 0
2.00	E=10	2.2	nE o	9	2	.65E	9.6	3.14E	9.0
2.50		2.8	5E 0	8		.29E	9.0	3.78E	0.8
3.00	E-10	3:4	2E 0	8	3	.83E	9.0	4.27E	90
5.00	E-10	4.3		8	4	48E	9.0	4.60E	90
8.00	E-10	3.1	7E 0	8	3	.07E	36	2.99E	9.0
1.00	E-09	2.2		8	2	. ZOE	9.8	2.088	90
1.50	E-09	1.0	6E 0	8	9	.83E	07	#.96E	07
2.00	E-09	5.2	4E 0	7	4	.76E	0.7	4.21E	97
2.50	E-09	2.8	5E n'	7	2	.55E	97	2.24E	07
3.00	E-09	1.7	2E 0'	7	1	.49E	97	1.31E	c 7
4.00	E-09	8.0	8E 0	5		.53E	06	5,648	CE
5.00	E-09	4.6	5E 0	b	3	.49E	06	3.96E	96
7.00	E-09	5.0	1E 0	6		.35E	06	1.115	06
1.00	E = 0 8	8.6	1E 01	5	ь	.75E	95	6.06E	05

Table 17 Stark Profiles for

	ARGON	1 XVII	I	Ly	•	T	=	4.6E6)	(DEG,	, K)	
	Ne	=	t .	00E	22	2		1.00E	: 2	3	5.01E	23
0.0	0E 00		6.	51E	98	3		4.97E	· 1	8	4.95E	9.0
	0E-11			47E	0.8	3		4.98E		8	4.93E	96
	0E-11			21E	0.8	3		4.875		8	4.84E	9.0
	0E-11			73E	08			4.68E			4.67F	9.0
	0E-11			15E	08	_		4.41		_	4.44E	90
	0E-10			26E	05			3.96			4.04E	30
	nE-10			73E	0.8			3.65E			3.76E	0.5
	0E-10			7E	08			3.218			3.36E	9.0
	0E-10			72E	9.8			2.96			3.13E	36
	0E-10			30E	28			2.638		_	2.838	0.5
	0E-10			34E	08			2.22E			2.46E	0.8
	0E-10			56E	0.8			1.95E			2.21E	0.8
	0E-10			9E	0.5			1.62E			1.93E	9.6
	1E-10			15E				1.70E				_
	0E-09				98						1.97E	0.8
				52E	0.5			1.67		_	1.88E	3.0
	0E-09			34E	08	_		1.355			1.33E	9.9
	nE-09			66E	07	_		9.09E			8.18E	07
	0E-09		-	19E	97			5.84E		_	4.94E	07
	0E-09			32E	0.7	_		3.788		_	3.07E	97
	1E-03) S E	υ 7			1.74E			1.36E	07
	0E-09			116	0.7			9.278		_	7.07E	0 É
	0E-09			23E	06)		3.53E		6	2.64E	96
1.0	0 E- 08		1 _ 5	55E	0.6			1.268	9.0	6	9.49E	0 =

Table 18 Stark Profiles for

ARGON XVI	III Ly	, T =	9.3E6	(DEG.	, r)	
α N _e =	1.00E	22	1.00E	23	5.00E	23
0.00E 00	8.26E	08	5.92E	9.6	5.46E	90
1.00E-11	8.18E	80	5.91E	98	5.44E	9.0
3.00E-11	7.62E	80	5.70E	98	5.30E	96
5.00E-11	6.69E	80	5.34E	08	5.03E	9.0
7.00E-11	5.68E	08	4.89E	9.0	4.68E	9.0
1.00E-10	4.32E	0.5	4.16E	38	4.10E	08
1.20E-10	3.61E	08	3.70E	98	3.72E	9.0
1.50E-10	2.80E	08	3.11E	08	3.21E	9.9
1.70E-10	2.41E	98	2.78E	n 8 n	2.91E	90
2.00E-10	1.97E	ე 5	2.39E	30	2.55E	g٤
2.50E-10	1.53E	80	1.93E	ŋ8	2.12E	9.0
3.00E-10	1.28E	0.8	1.64E	98	1.84E	9.0
5.00E-10	1.09E	98	1.33E	28	1.54E	0.8
8.00E-10	1.30E	98	1.46E	30	1.65E	30
1.00E-09	1.40E	48	1.528	9e	1.67E	0.8
1.50E-09	1.31E	05	1.34E	96	1.36E	08
2.00E-09	9.35E	07	9.64E	97	9.23E	07
2.50E-09	6.80E	07	6.48E	97	5.95E	97
3.00E-09	4.62E	07	4.33E	97	3.86E	07
4.00E-09	2.23E	27	2.05E	07	1.77E	07
5.00E-09	1.21E	07	1.17E	17	9.29E	06
7.00E-09	4.79E	06	4.19E	36	3.43E	16
1.00E-08	1.95E	96	1.49E	1)6	1.16E	0.6

Table 19
Stark Profiles for
ARGON XVIII LS. T = 4.6E6 (DEG. K)

N _e =	1.00E	22	1.00E	23	5.00E	23
≪ ✓e	-			_		_
0.00E 00	7.35E	07	9.67E	υ7	1.14E	0.6
1.00E-11	7.35E	07	9,68E	07	1.17E	30
3.00E-11		07	9.73E	07	1.15E	30
5.00E-11		07	9.84E	97	1.17E	9.0
7.00E-11		07	9.99E	07	1.17E	9.0
1.00E-10		07	1.03E	0.8	1.25E	9.0
1.20E-10		97	1.06E	0.8	1.27E	90
1.50E-10		07	1.19E	0.8	1.37E	0.5
1.70E-10		07	1.13E	9.0	1.43E	9.6
2.00E-10		07	1.19E	98	1,52E	08
2,50E-10		98	1.29E	9.0	1.67E	90
3.0CE-10		0.8	1.37E	98	1.82E	9.0
5.00E-10		98	1.70E	08	2.16E	ŋ B
8.005-10		08	1.71E	08	1.96E	98
1.00E-09		98	1.56E	98	1.71E	30
1.508-09		08	305.1	96	1.28E	30
2.005-09		ŏ7	9.71E	27	9 87E	07
2.508-09		97	7.72E	07	7.30E	17
3.00E-09		07	5.97E	07	5.24E	07
4.00E-09		07	3.49E	07	2.65E	07
5.00E-07		07	1.94E	07	1.40E	97
7.00E-07	9.88E	06	7.528	06	5.11E	96
	3.64E	06	3.578	96	1.76E	06
1.00E-08	3 6 0 7 6	J J		, 0	- 6 - 4 -	~ •

Table 20 Stark Profiles for

ARGON	XVIII L	•	7 = 9.3E6		(DEG. K)	
\propto N _e =	1.00E	22	1.00E	23	5.008	23
0.00E 00	5.60E	07	7.30E	07	8.05E	97
1.00E-11	5.60E	07	7.30E	07		97
3.00E-11	5.65E	07	7.35E	07		07
5.00E-11	5.74E	07	7.458	07		07
7.00E-11	5.88E	07	7.59E	37		07
1.00E-10	6.16E	07	7.88E	97		07
1.20E-10	6.40E	07	8.13E	97		07
1.50E-10	6.81E	07	8.56E	0.7	-	07
1.70E-10	7.13E	07	8.88E	07		9.0
2.00E-10	7.64E	97	9.41E	97		30
2.50E-10	8.62E	07	1.04E	0.9		30
3.00E-10	9.67E	97	1.14E	98		30
5.09E-10	1.35E	28	1.508	98		30
8.00E-10	1.54E	03	1.61E	08		9.0
1.00E-03	1.45E	08	1.50E	08		96
1.50E-09	1.12E	80	1.16E	28		9.0
2.00E-09	9.20E	07	9.48E	07		07
2.50E=09	7.73E	07	7.82E	97		07
3.00E-09	6.39E	07	6.27E	07	-	07
4.00E-09	4.09E	07	3.83E	07		97
5.00E-09	2.55E	07	2.30E	37		97
7.00E-09	1.10E	07	9,33E	06		96
1.00E-05	4.14E	06	3.33E	06		06

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